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# Galaxy mass profiles from strong lensing – III. The two-dimensional broken power-law model

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# ABSTRACT

When modelling strong gravitational lenses, i.e. where there are multiple images of the same source, the most widely used parametrization for the mass profile in the lens galaxy is the singular power-law model  $\rho(r) \propto r^{-\gamma}$ . This model may be insufficiently flexible for very accurate work, for example, measuring the Hubble constant based on time delays between multiple images. Here, we derive the lensing properties – deflection angle, shear, and magnification – of a more adaptable model where the projected mass surface density is parametrized as a continuous two-dimensional broken power law (2DBPL). This elliptical 2DBPL model is characterized by power-law slopes  $t_1$  and  $t_2$  either side of the break radius  $\theta_B$ . The key to the 2DBPL model is the derivation of the lensing properties of the truncated power-law (TPL) model, where the surface density is a power law out to the truncation radius  $\theta_T$  and zero beyond. This TPL model is also useful by itself. We create mock observations of lensing by a TPL profile where the images form outside the truncation radius, so there is no mass in the annulus covered by the images. We then show that the slope of the profile interior to the images may be accurately recovered for lenses of moderate ellipticity. This demonstrates that the widely held notion that lensing measures the slope of the mass profile in the annulus of the images, and is insensitive to the mass distribution at radii interior to the images, is incorrect.

**Key words:** gravitational lensing: strong – galaxies: general.

# **1 INTRODUCTION**

This is the third in a series of papers examining how strong gravitational lensing of an extended source may be used to measure the profile of the projected surface mass density in the lens, using lensing data alone, independent of dynamics. In the first and second papers in the series (O'Riordan, Warren & Mortlock 2019, 2020, hereinafter Paper I and Paper II), we examined, respectively, the circular and elliptical cases of the singular power-law (SPL) lens, with 3D density profile  $\rho(r) \propto r^{-\gamma}$ . The model projects to a power law in surface mass density with exponent  $t = \gamma - 1$ . We used synthetic observations to determine the constraints on  $\gamma$  for a wide range of image configurations, and we developed a theoretical understanding of how the different observables, positions, and fluxes, contribute to the constraints on  $\gamma$  in the various configurations. We showed that in the best cases the slope may be measured to an accuracy  $\sigma_{\gamma} \simeq 0.01$ .

Having shown that strong lensing observations on their own can provide accurate measurements of the slope, we now turn to the question of where in the radial profile these constraints apply. In the SPL model, the shape of the surface density profile is quantified by a single parameter, the power-law exponent  $\gamma$ , or equivalently *t*. In this paper, we introduce a more versatile mass model with the goal of determining the constraints on the lens surface density as a

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function of projected radius. We define an elliptical model in which the surface density is a continuous broken power law (BPL). This two-dimensional BPL (2DBPL) model has two extra parameters compared to the SPL model: it is specified by an inner powerlaw slope  $t_1$ , an outer power-law slope  $t_2$ , and a break (elliptical) radius  $\theta_B$ . In this paper, we derive the main useful lensing properties of this model i.e. the deflection angle and the shear, and thereby the magnification. In the next paper in the series, we will explore the constraints on the parameters  $t_1$ ,  $t_2$ , and  $\theta_B$  for different image configurations.

The 2DBPL model, parametrizing the surface density, is closely related to the 3DBPL model, parametrizing the density, for which the lensing properties have been derived by Du et al. (2020). The 3D model could be a physical model for a real galaxy, while the 2D model cannot be exactly, since no 3D ellipsoidal density distribution can project to a 2DBPL profile. The projection of the 3DBPL model to 2D results in a softened break between the two power laws. The original reason for developing the 2DBPL model was to have a distinct change in slope as a means of directly contrasting the model either side of the break. In this way by comparing the uncertainties on the two slopes it will be possible to gain an understanding of how lensing constrains the mass profile in the most direct manner.

Although created as a theoretical tool to understand how lensing constrains the mass profile, the 2DBPL profile is also useful as a functional form for fitting real lenses as it represents the simplest extension beyond the commonly used SPL model. By using Bayesian model comparison techniques it will be possible to determine if such an extension beyond the SPL model, with two extra parameters, is justified by the data. An accurate mass model is a critical component of any lensing study but this is especially true for time delay cosmography, where the delays in light traveltime between the multiple images in a single system are used to constrain the Hubble constant (e.g. Wong et al. 2020). A number of authors have suggested that the currently employed SPL model lacks the freedom necessary to model accurately the lens mass when measuring  $H_0$  (Xu et al. 2016; Sonnenfeld 2018; Kochanek 2020). The consequence could be that measurements of  $H_0$ , although precise, are inaccurate because of a biased measurement of the potential at the positions of the lensed images.

The lensing properties of the 2DBPL profile are derived by first determining the lensing properties of the 2D truncated power-law (2DTPL) profile, where the surface density is represented by a singular power-law profile out to a specified radius, and then zero beyond. The 2DBPL profile is then constructed by combining SPL and 2DTPL profiles in a straightforward way (explained below). The derivation of the lensing properties of the 2DTPL model is therefore the main theoretical innovation presented in this paper.

For the remainder of the paper, we refer to the 2DTPL and 2DBPL models simply as the TPL and BPL models for the sake of readability.

Regarding measurements of the mass profile, it is widely stated or implied that lensing images constrain the slope of the profile only over the annulus spanned by the images, i.e. near the Einstein radius, and provide no useful information on the mass profile interior to the innermost image (Kochanek 1995, 2006; Koopmans et al. 2006; van de Ven, Mandelbaum & Keeton 2009; Treu 2010; Chae, Bernardi & Kravtsov 2014; Hezaveh et al. 2016; Suyu et al. 2017; Spingola et al. 2018). The clearest example of this sentiment is in Kochanek (2006) where it is stated 'it is important to remember that the actual constraints on the density structure really only apply over the range of radii spanned by the lensed images'. In this paper, we use the TPL model to examine this belief. We construct mock observations for elliptical lenses where the images form outside the truncation radius. In these observations, there is therefore no mass in the annulus spanned by the lensed images. We then fit the TPL model to the mock observations to determine the constraints on the power-law slope for different image configurations.

The paper is organized as follows. In Section 2, we present the theory for the TPL model. In Section 3, we formulate the BPL model and in Section 4 we provide a numerical recipe for fast computation of the deflection angle for the TPL and BPL models. In Section 5, we use the TPL model to examine if the slope interior to the images can be constrained. Conclusions are presented in Section 6.

#### 2 TRUNCATED POWER-LAW MASS MODEL

Before deriving the lensing properties for the BPL, we first derive them for a simpler model, the TPL. These results will be useful in formulating the BPL in Section 3.

#### 2.1 Convergence

In the TPL model, the surface density is described by a power-law interior to some elliptical radius called the truncation radius and is zero outside this radius. Explicitly, the convergence in the TPL model is

$$\kappa(\theta_{\varepsilon}) = \begin{cases} \kappa_{\mathrm{T}}(\theta_{\mathrm{T}}/\theta_{\varepsilon})^{t}, & \text{for } \theta_{\varepsilon} \leq \theta_{\mathrm{T}} \\ 0, & \text{for } \theta_{\varepsilon} > \theta_{\mathrm{T}}, \end{cases}$$
(1)

where  $\theta_{\rm T}$  is the truncation radius,  $\kappa_{\rm T}$  is the convergence at  $\theta_{\rm T}$ , and *t* is the logarithmic slope. The elliptical radius  $\theta_{\varepsilon}$  is defined

$$\theta_{\varepsilon}^2 = q^2 \theta_1^2 + \theta_2^2, \tag{2}$$

where q is the axial ratio of the minor to major axes of the mass distribution's isodensity contours, and is related to ellipticity  $\varepsilon$  by  $q = 1 - \varepsilon$ .

Equation (1) also includes a normalization  $\kappa_{\rm T}$  which we now define. We wish to relate  $\kappa_{\rm T}$  to the scale length *b* such that *b* retains its usual meaning from the single power-law model; that the average density inside the elliptical radius *b* is the critical density  $\Sigma_{\rm c}$ . If  $M(\theta)$  is the mass enclosed by a radius  $\theta$ , then at  $\theta = b$  we require

$$M(b) = \sum_{\rm c} \pi b^2 D_{\rm d}^2 / q, \tag{3}$$

where  $D_d$  is the distance to the lens. In general, for an elliptical mass distribution the total mass enclosed by a radius  $\theta_{\varepsilon}$  is

$$M(\theta_{\varepsilon}) = \frac{\sum_{c} D_{d}^{2}}{q} \int_{0}^{\theta_{\varepsilon}} \kappa \left(\theta_{\varepsilon}^{\prime}\right) 2\pi \theta_{\varepsilon}^{\prime} \mathrm{d}\theta_{\varepsilon}^{\prime}. \tag{4}$$

Using equation (1), for a radius  $\theta_{\varepsilon} > \theta_{T}$  the mass enclosed is a constant;

$$M\left(\theta_{\varepsilon} > \theta_{\mathrm{T}}\right) = \frac{2\pi\Sigma_{\mathrm{c}}D_{\mathrm{d}}^{2}\kappa_{\mathrm{T}}\theta_{\mathrm{T}}^{2}}{q(2-t)}.$$
(5)

To find  $\kappa_{\rm T}$ , we can then combine equations (5) and (3) to obtain

$$\kappa_{\rm T} = \begin{cases} \frac{2-t}{2\nu^2}, & \text{for } \nu \le 1, \\ \frac{2-t}{2\nu^t}, & \text{for } \nu \ge 1, \end{cases}$$
(6)

where  $v = \theta_{\rm T}/b$ .

#### 2.2 Deflection angle

To find the deflection angle for the TPL model, we follow initially the same route used by Tessore & Metcalf (2015, hereafter TM15) for the SPL model, and adopt the same notation where the complex image plane coordinate is  $z = \theta_1 + i\theta_2$  and the complex deflection angle is  $\alpha = \alpha_1 + i\alpha_2$ . Bourassa & Kantowski (1975) give the deflection angle for a general elliptical mass profile as

$$\alpha^*(z) = \frac{2}{qz} \int_0^{\theta_\varepsilon(z)} \kappa(\theta) \theta\left(1 - q' \frac{\theta^2}{z^2}\right)^{-1/2} \mathrm{d}\theta,\tag{7}$$

where  $q' = (1 - q^2)/q^2$ . Inserting equation (1), we have

$$\alpha^*(z) = \frac{2\kappa_{\rm T}\theta_{\rm T}^t}{qz} \int_0^{\theta'} \theta^{1-t} \left(1 - q'\frac{\theta^2}{z^2}\right)^{-1/2} \mathrm{d}\theta,\tag{8}$$

with

$$\theta' = \begin{cases} \theta_{\varepsilon}(z), & \text{for } \theta_{\varepsilon}(z) \le \theta_{\mathrm{T}}, \\ \theta_{\mathrm{T}}, & \text{for } \theta_{\varepsilon}(z) > \theta_{\mathrm{T}}. \end{cases}$$
(9)

First, consider the deflection angle outside  $\theta_T$  for a circular mass distribution, i.e. with q = 1. Equation (8) is then easy to evaluate and gives

$$\alpha^*(z) = \frac{b^2}{z}.$$
(10)

This is the same as for a point mass with Einstein radius  $\theta_E = b$ . As expected, the deflection angle exterior to the truncation radius does not depend on the distribution of mass interior, via *t* or otherwise, when the lens is circular.

Now we consider the elliptical case, i.e. for a general  $q \neq 1$ . Following TM15, we take advantage of the fact that an integral of the form

$$I(\theta, t; z) = \int_0^\theta \theta'^{1-t} \left(1 - q' \frac{\theta'^2}{z^2}\right)^{-1/2} \mathrm{d}\theta'$$
(11)

has the solution

$$I(\theta, t; z) = \frac{\theta^{2-t}}{2-t} F(\theta, t; z), \qquad (12)$$

where

$$F(\theta, t; z) = {}_{2}F_{1}\left(\frac{1}{2}, 1 - \frac{t}{2}; 2 - \frac{t}{2}; q'\frac{\theta^{2}}{z^{2}}\right),$$
(13)

and  $_2F_1$  is the Gaussian hypergeometric function. Equation (8) then becomes

$$\alpha^{*}(z) = \frac{b^{2}}{qz} \times \begin{cases} F(\theta_{\varepsilon}, t; z) \left(\frac{\theta_{\mathrm{T}}}{\theta_{\varepsilon}}\right)^{t-2}, & \text{for } \theta_{\varepsilon}(z) \leq \theta_{\mathrm{T}}, \\ F(\theta_{\mathrm{T}}, t; z), & \text{for } \theta_{\varepsilon}(z) \geq \theta_{\mathrm{T}}. \end{cases}$$
(14)

The deflection angle exterior to the truncation radius has now picked up a dependence on the mass distribution interior, through *t* in the hypergeometric function. For the case  $\theta_{\varepsilon} \leq \theta_{\rm T}$ , the deflection angle is identical to the final line of TM15's equation (11) up to a factor of  $\nu^{2-t}$  which accounts for the mass deficit inside *b* when  $\nu < 1$ . This factor ensures that *b* retains the same meaning for both the TPL and SPL even though they are differently normalized, i.e. a source at  $\beta$ = 0 will form a ring at  $\theta_{\varepsilon} = b$  when q = 1 in both models. The result in the  $\theta_{\varepsilon}(z) < \theta_{\rm T}$  case could be further simplified by separating the radial and angular parts (see TM15's equation 12 onwards). In the  $\theta_{\varepsilon}(z) > \theta_{\rm T}$  case,  $\alpha$  does not benefit from the same simplifications because the mass profile is only integrated up to  $\theta_{\rm T}$  in equation (8), rather than all the way up to *z*. Note that the deflection angle is continuous across the boundary at  $\theta_{\rm T}$ , even though the mass profile is not.

The sensitivity of the deflection angle outside  $\theta_{T}$  to the slope inside  $\theta_{\rm T}$  is illustrated in Fig. 1. The quantity  $\Delta \alpha$ , as a fraction of b, is calculated at the point at elliptical radius b on the diagonal line  $\theta_1 = \theta_2$ .  $\Delta \alpha$  is the magnitude of the change in the deflection angle vector for a change in slope of  $\Delta t = 0.1$  around an isothermal, i.e. t = 1 slope. The figure shows how the sensitivity depends on two features of the lens. First, the deflection angle is more sensitive to the mass interior as the truncation radius approaches the Einstein radius, i.e. as  $\nu = \theta_{\rm T}/b \rightarrow 1$ . For a very small truncation radius, the dependence vanishes entirely, and as  $\nu \to 1$  the quantity  $\Delta \alpha$  in the figure converges to that of the SPL. Second, the dependence is stronger for higher ellipticities. This could have been predicted from the results of Paper II, where we found that in general more elliptical lenses provide better constraints on the mass profile slope. The large increase in sensitivity between q = 0.99, essentially a circular lens, and q = 0.9 indicates that the images should be sensitive to the interior slope even for small ellipticities. We will examine both of these effects in more detail in the next paper in this series.

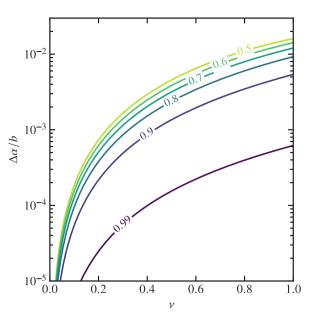
#### 2.3 Shear and magnification

The complex shear  $\gamma(z)$  is defined as

$$\gamma^*(z) = \frac{\partial \alpha^*}{\partial z},\tag{15}$$

where  

$$\frac{\partial}{\partial z} = \frac{1}{2} \left( \frac{\partial}{\partial \theta_1} - i \frac{\partial}{\partial \theta_2} \right), \qquad (16)$$



**Figure 1.** The sensitivity of the deflection angle to small changes in slope as a function of  $v = \theta_T/b$ . The sensitivity is calculated along the line  $\theta_1 = \theta_2$  at the scale radius  $\theta_{\varepsilon} = b$ . Each curve represents a different axial ratio running from an (almost) circular lens to q = 0.5.

is the Wirtinger derivative. The shear interior to the truncation radius is just that for the single power law, given by TM15's equation (16) but with our definitions of  $\kappa$  and  $\alpha$ . Exterior to the truncation radius, we use the result

$$\frac{\partial}{\partial z}F(\theta,t;z) = \frac{2-t}{z} \left[ F(\theta,t;z) - \left(1 - q'\frac{\theta^2}{z^2}\right)^{-1/2} \right],\tag{17}$$

to find

$$\gamma^{*}(z) = \begin{cases} (1-t)\frac{\alpha^{*}(z)}{z} - \frac{z^{*}}{z}\kappa(z), & \text{for } \theta_{\varepsilon}(z) \leq \theta_{\mathrm{T}}, \\ (1-t)\frac{\alpha^{*}(z)}{z} - \frac{2-t}{z^{2}}\left(1-q'\frac{\theta_{\mathrm{T}}^{2}}{z^{2}}\right)^{-1/2} & \text{for } \theta_{\varepsilon}(z) \geq \theta_{\mathrm{T}}. \end{cases}$$

$$(18)$$

Having defined both the convergence and shear it is possible to compute the scalar magnification from the standard relation

$$\mu^{-1} = (1 - \kappa)^2 - |\gamma|^2.$$
<sup>(19)</sup>

## 2.4 Lensing potential

Inside the truncation radius, the potential is simply that due to a single power law which TM15 gives as

$$\psi(z) = \frac{z\alpha^{*}(z) + z^{*}\alpha(z)}{2(2-t)},$$
(20)

where  $\alpha^*(z)$  is given by equation (14). The potential outside the truncation radius due to the mass interior can be found by summing the contributions from infinitesimally thin, homoeoidal, concentric elliptical rings each of constant density. From Schramm (1990), we get the potential for such a ring at a position *z* outside the ring

$$\psi(z) = \frac{2}{q} \kappa(\theta_{\varepsilon}) \theta_{\varepsilon} \cosh^{-1}\left(\frac{zq}{\theta_{\varepsilon} \sqrt{1-q^2}}\right) \mathrm{d}\theta_{\varepsilon},\tag{21}$$

where q is the axial ratio of the ring, in this case constant across all rings,  $\kappa$  is the surface density of the ring, and  $\theta_{\varepsilon}$  is the elliptical radius of the ring defined in equation (2). Using equation (1), we can then find the potential for the mass inside  $\theta_T$  with the integral

$$\psi(z) = \frac{2\kappa_{\rm T}\theta_{\rm T}^t}{q} \left[ \int_0^{\theta_{\rm T}} \theta^{1-t} \cosh^{-1} \left( \frac{zq}{\theta\sqrt{1-q^2}} \right) \mathrm{d}\theta \right] - C_{\rm T}, \quad (22)$$

which must be evaluated numerically. The constant  $C_{\rm T}$  ensures the potential is continuous across  $\theta_{\rm T}$ . Explicitly this is  $C_{\rm T} = \psi_{\theta_{\rm c} > \theta_{\rm T}}(z_{\rm T}) - \psi_{\theta_{\rm c} < \theta_{\rm T}}(z_{\rm T})$ , where each  $\psi$  is given by equations (20) and (22), respectively, and  $z_{\rm T}$  is an arbitrary point at the truncation radius, e.g.  $z_{\rm T} = i\theta_{\rm T}$ .

#### **3 BROKEN POWER-LAW MASS MODEL**

We can make use of the results for the TPL to formulate a more useful model, a two-dimensional continuous BPL. The BPL model that follows is implemented in the lens modelling software PYAUTOLENS (Nightingale, Dye & Massey 2018).

#### 3.1 Convergence

We define the convergence for a BPL projected mass density profile as

$$\kappa(\theta_{\varepsilon}) = \begin{cases} \kappa_{\mathrm{B}}(\theta_{\mathrm{B}}/\theta_{\varepsilon})^{t_{1}}, & \text{for } \theta_{\varepsilon} \leq \theta_{\mathrm{B}}, \\ \kappa_{\mathrm{B}}(\theta_{\mathrm{B}}/\theta_{\varepsilon})^{t_{2}}, & \text{for } \theta_{\varepsilon} \geq \theta_{\mathrm{B}}. \end{cases}$$
(23)

where  $\theta_{\rm B}$  is the break radius,  $\kappa_{\rm B}$  is the convergence at the break radius, and  $t_1$  and  $t_2$  are the inner and outer 2D logarithmic slopes, respectively. Inserting equation (23) into equation (4) gives an expression for  $\kappa_{\rm B}$ ,

$$\kappa_{\rm B} = \begin{cases} \frac{2 - t_1}{2\nu^2 \left[1 + \delta_t \left(\nu^{t_2 - 2} - 1\right)\right]}, & \text{for } \nu < 1, \\ \frac{2 - t_1}{2\nu^{t_1}}, & \text{for } \nu \ge 1, \end{cases}$$
(24)

where  $\nu$  now has the definition  $\nu = \theta_{\rm B}/b$  and we define

$$\delta_t = \frac{2-t_1}{2-t_2}.\tag{25}$$

#### 3.2 Deflection angle

We can find the deflection angle from equation (7). The solution contains integrals of the form in equation (11) which we use to simplify the results.

For positions inside the break radius, i.e. where  $\theta_{\varepsilon} \leq \theta_{B}$ , we find

$$\alpha^*(z) = \frac{2\kappa_{\rm B}}{2-t_{\rm I}} \frac{\theta_{\rm B}^2}{qz} \left(\frac{\theta_{\rm B}}{\theta_{\varepsilon}}\right)^{t_{\rm I}-2} F(\theta_{\varepsilon}, t_{\rm I}; z), \tag{26}$$

which is just the deflection angle for a power law of slope  $t_1$  with an adjusted normalization. Outside the break radius, i.e. where  $\theta_{\varepsilon} \ge \theta_B$ , we have

$$\alpha^{*}(z) = \frac{2\kappa_{\rm B}}{2-t_{\rm I}} \left\{ \frac{\theta_{\rm B}^{2}}{qz} F(\theta_{\rm B}, t_{\rm I}; z) + \delta_{t} \left[ \frac{\theta_{\rm B}^{2}}{qz} F(\theta_{\varepsilon}, t_{\rm 2}; z) \left( \frac{\theta_{\rm B}}{\theta_{\varepsilon}} \right)^{t_{2}-2} - \frac{\theta_{\rm B}^{2}}{qz} F(\theta_{\rm B}, t_{\rm 2}; z) \right] \right\}, \quad (27)$$

which can be further simplified if  $\nu < 1$  using equation (24) for  $\kappa_{\rm B}$ . Writing the deflection angle in this way is useful because it makes its three constituent parts clear. Comparing with equation (14), we see that  $\alpha(z)$  for the BPL can be found by combining three simpler deflection angles. We add  $\alpha$  for a power law with the inner slope  $t_1$  truncated at  $\theta_B$  and  $\alpha$  for a single power law with the outer slope  $t_2$  (first and second terms). We then subtract the contribution from the single power law with slope  $t_2$  inside the break radius (third term).

We can check the result for the case where both slopes are the same, i.e. when  $t_1 = t_2 = t$ . In this case, the normalization becomes

$$\kappa_{\rm B} = \frac{2-t}{2\nu^t}.$$
(28)

We also have  $\delta_t = 1$  and so the first and third hypergeometric terms in equation (27) cancel out. Both equations (26) and (27) reduce to

$$\chi^*(z) = \frac{b^2}{qz} \left(\frac{b}{\theta_{\varepsilon}}\right)^{t-2} F(\theta_{\varepsilon}, t; z),$$
(29)

which is identical to TM15's equation (11), i.e. the deflection angle for a single power law.

#### 3.3 Shear

We find the shear for the BPL by using equations (26) and (27) with the definition of complex shear in equation (15). For the case where  $\theta_{\varepsilon} < \theta_{\rm B}$ , we have

$$\gamma^*(z) = \frac{2\kappa_{\rm B}\nu^{t_1}}{2 - t_1} \,\gamma^*_{t_1}(z),\tag{30}$$

where  $\gamma_t^*(z)$  is the shear due to a single power law with slope *t*, given by

$$\gamma_t^*(z) = (1-t)\frac{\alpha_t^*(z)}{z} - \kappa(z)\frac{z^*}{z},$$
(31)

with  $\alpha_t^*(z)$  given by equation (29). Outside the break radius, when  $\theta_{\varepsilon} > \theta_{\rm B}$ , the shear is

$$\gamma^{*}(z) = \frac{2\kappa_{\rm B}}{2-t_{\rm I}} \left\{ \frac{\theta_{\rm B}^{2}}{qz^{2}} \left[ \frac{t_{\rm I} - t_{\rm 2}}{\sqrt{1 - q'\theta_{\rm B}^{2}/z^{2}}} + (1 - t_{\rm I})F(\theta_{\rm B}, t_{\rm I}; z) - (1 - t_{\rm 2})F(\theta_{\rm B}, t_{\rm 2}; z) \right] + \nu^{t_{\rm 2}}\delta_{t}\gamma_{t_{\rm 2}}^{*}(z) \right\}.$$
(32)

Comparing with the shear for the truncated profile in equation (18), we see that the shear for the BPL has the same composition as described for the deflection angle in the previous section.

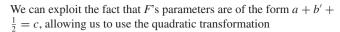
#### **4 COMPUTATION**

To perform Markov chain Monte Carlo (MCMC) fitting to image planes using either the TPL or BPL, we need a method to efficiently compute the deflection angles in equations (14), (26), and (27). In the case of both models, all that is required is a method for computing our specific hypergeometric function *F* in equation (13). We pursue a similar approach to that of TM15 for the SPL, however, in this work we cannot simplify the final argument of *F* in the same way and so we require a slightly different recipe for computation. In TM15, the  $\theta$  used in *F* is simply  $\theta_{\varepsilon}(z)$  which allows for some simplification using their definition of  $z = \theta_{\varepsilon} e^{i\phi}$ , where  $\phi$  is an elliptical angle. In this work, we must be able to use the constants  $\theta_{\rm B}$  or  $\theta_{\rm T}$  in place of  $\theta_{\varepsilon}(z)$ , prohibiting the same simplifications.

Recall that we defined

$$F(\theta, t; z) = {}_{2}F_{1}\left(\frac{1}{2}, 1 - \frac{t}{2}; 2 - \frac{t}{2}; q'\frac{\theta^{2}}{z^{2}}\right).$$
(33)

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$${}_{2}F_{1}\left(a,b';a+b'+\frac{1}{2},z'\right)$$
  
=  ${}_{2}F_{1}\left(2a,2b';a+b'+\frac{1}{2},\frac{1-\sqrt{1-z'}}{2}\right),$  (34)

(Bateman 1955). Under this transformation, F becomes

$$F(\theta, t; z) = {}_{2}F_{1}\left[1, 2 - t; 2 - \frac{t}{2}; u(\theta; z)\right],$$
(35)

where

$$u(\theta; z) = \frac{1 - \sqrt{1 - q'\theta^2/z^2}}{2}.$$
(36)

With the condition that |u| < 1, we can use the series representation of  ${}_{2}F_{1}$ , as follows:

$$F(\theta, t; z) = \sum_{n=0}^{\infty} a_n(t) u(\theta; z)^n,$$
(37)

where

$$a_n(t) = \frac{\Gamma(n+1)}{n!} \frac{\Gamma(2-t+n)}{\Gamma(2-t/2+n)} \frac{\Gamma(2-t/2)}{\Gamma(2-t)}.$$
(38)

The quadratic transformation ensures that |u| only exceeds unity for very extreme axial ratios. For axial ratios  $q \leq 0.32$ , there are regions in the image plane where |u| > 1 and the method does not produce accurate results. For our purposes, however, the range of axial ratios  $0.32 < q \leq 1$  is more than sufficient.

By using the fact that  $\Gamma(z + 1) = z\Gamma(z)$ , we find a relatively simple recurrence relation between consecutive coefficients

$$\frac{a_{n+1}}{a_n} = \frac{2n+4-2t}{2n+4-t},\tag{39}$$

and  $a_0(t) = 1$ . This leaves us with a straightforward recipe for computing  $\alpha$  in the BPL with

$$\alpha^*(z) = \frac{2\kappa_{\rm B}}{qz} \frac{\theta_{\rm B}^2}{2-t_1} \left(\frac{\theta_{\rm B}}{\theta_{\varepsilon}}\right)^{t_1-2} \sum_{n=0}^{\infty} a_n(t_1) \, u(\theta_{\varepsilon}; z)^n,\tag{40}$$

for  $\theta_{\varepsilon} \leq \theta_{\rm B}$ , and

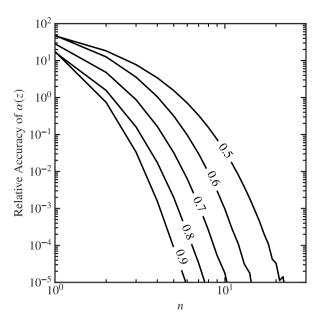
$$\alpha^{*}(z) = \frac{2\kappa_{\rm B}}{qz} \frac{\theta_{\rm B}^{2}}{2 - t_{\rm I}} \sum_{n=0}^{\infty} \left\{ u(\theta_{\rm B}; z)^{n} \left[ a_{n}(t_{\rm I}) - \delta_{t} a_{n}(t_{\rm 2}) \right] + u(\theta_{\varepsilon}; z)^{n} \left( \frac{\theta_{\rm B}}{\theta_{\varepsilon}} \right)^{t_{2} - 3} \delta_{t} a_{n}(t_{\rm 2}) \right\},$$
(41)

for  $\theta_{\varepsilon} > \theta_{\rm B}$ .

Fig. 2 shows the relative accuracy of the method as the number of coefficients *n* increases. In this case, the relative accuracy is the maximum (over a  $100 \times 100$  pixel 6 arcsec wide image plane) relative difference between the computed deflection angle using *n* coefficients and the same with n = 100. Computation time increases linearly with the number of coefficients.

# **5 CONSTRAINING THE SLOPE INTERIOR TO THE IMAGES**

We now return to the TPL model developed in Section 2 and its primary use in addressing a central question in this series of papers: what constraints, if any, can one obtain on the mass distribution interior to the lensed images? For a circular TPL model, the deflection



**Figure 2.** The relative accuracy of equation (37) for different values of *n*. Each line corresponds to a different axial ratio, which is labelled.

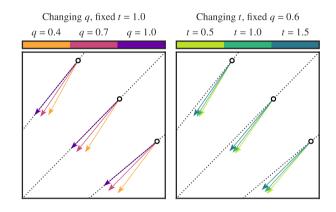


Figure 3. The effect of the axial ratio q and the slope t on the deflection angle in a truncated lens. The vectors are the deflection angle (not to scale) at three points near the Einstein radius in the upper right quadrant of the image plane. The truncation radius is inside these points. The dotted lines intersect the centre of the lens.

angle outside  $\theta_T$  has no dependence on the mass profile interior to  $\theta_T$  (see equation 10). The lensing potential outside any circularly symmetric mass distribution is that of a point mass at the centre. However, this does not hold for elliptical mass distributions.

As a thought experiment, consider the potential  $\psi(z)$  and the deflection angle  $\alpha(z)$  at a point z outside the truncation radius, and not lying on a principal axis, as in Fig. 3. For a circular lens, the vector points towards the centre of the lens. This is the case in the left-hand panel of Fig. 3 when q = 1, t = 1, and is obvious from equation (10). As the ellipticity increases the deflection angle points away from the centre and towards the lens's semimajor axis, or the x-axis in the figure. Increasing (decreasing) the ellipticity decreases (increases) the circularity of the potential  $\psi(z)$  and, because  $\alpha = \partial \psi/\partial z$ , the deflection angle changes direction accordingly.

Increasing the ellipticity, but keeping the same total mass inside  $\theta_{T}$ , moves mass from the centre to the region around the semimajor axis. In principle, a similar result can be achieved by changing the slope *t*. Increasing *t* concentrates mass in the centre of the lens, circularizing

the potential and the deflection angle points more towards the centre as a result. Conversely, decreasing t pushes mass towards the edge of the lens and the potential also becomes more elliptical. This behaviour is clear in the right-hand panel of Fig. 3.

This thought experiment raises two interesting points. First, for an elliptical lens with multiple images exterior to the truncation radius, the deflection angle at the images must be sensitive to the slope in the centre. Second, both the slope t and the axial ratio q can be used as we described to modify the angular structure in the potential. For small changes in either variable, these modifications should look very similar. We therefore expect t and q to be correlated.

Rather than restrict ourselves to this thought experiment, we can perform an actual experiment using the TPL model we developed in Section 2. We construct a number of mock observations with the technique used elsewhere in the series. The details of this procedure are in section 3 of Paper I. The fidelity of the procedures for creating mock observations has been confirmed by the good agreement between parameters and their uncertainties derived from analysis of the mock observations and the predictions of theory (Paper I; Paper II).

We created mock observations with the TPL model, ensuring that in all cases the images form outside the truncation radius. This ensures that in the annulus spanned by the images there is no mass whatsoever, and likewise, in the region where there is mass, there are no images.<sup>1</sup> All mock observations have the same total signal-tonoise ratio in the images S = 100. S is defined such that only pixels that belong to lensed images, found by a masking procedure, are included in the calculation (see Paper I, section 3.3). This means that the ability of different lens configurations to constrain parameters can be compared in an equal manner, independently of the magnification. Our mock observations use a similar set of parameters to those for the circular and elliptical SPLs in previous papers. We have  $b = \sqrt{q}$ , t = 1 (equivalent to  $\gamma = 2$ ), and use a Sérsic source with index  $n_s = 2$ .

Examples of mock observations are provided in the top row of Fig. 4, with q decreasing, ellipticity increasing, left to right. The dashed ellipse marks the truncation radius in each case. The images produced by the TPL model are both significantly thinner and significantly more circular in nature compared to the SPL model with the same parameters. These images could be directly compared with, for example, fig. 2 of Paper II. The potential for the TPL model is both steeper than in the SPL and circularizes faster. The result is a smaller radial magnification and a more 'full' Einstein ring between the images, because the caustic is smaller.

We used ensemble MCMC sampling to fit two different models to the data. These both use the TPL profile to model the mass and a Sérsic profile to model the source. In the first case, Case 1, the truncation radius is fixed to the true value. In Case 2, the truncation radius is a free parameter. Case 1 and Case 2 have 11 and 12 parameters, respectively. For each case, there are seven parameters for the source: position  $\beta_x$  and  $\beta_y$ , size  $r_{\text{eff.}}$ , brightness  $I_0$ , Sérsic index  $n_s$ , axial ratio  $q_s$ , and position angle  $\phi_s$ . Both models have four lens parameters in common: lensing strength *b*, mass profile slope *t*, axial ratio *q*, and position angle  $\phi_L$ . Case 2 has the extra parameter  $\theta_T$ .

The results of fitting to the mock observations are provided in Fig. 4, plotting posterior probability contours in a corner plot of the interesting parameters, i.e. *t* and *q* for Case 1 (middle row), and *t*, *q*, and  $\theta_{\rm T}$  for Case 2 (bottom row). To check the goodness of fit of the recovered parameter values, we compare the mock observations with the best-fitting model, made using the median sample values from the posteriors in Fig. 4. For a large number of degrees of freedom  $N_{\rm dof}$ ,  $\chi^2$  is normally distributed with mean  $N_{\rm dof}$  and standard deviation  $\sqrt{2N_{\rm dof}}$ . Therefore, if the model is a good fit to the data, one expects the quantity  $(\chi^2 - N_{\rm dof}) / \sqrt{2N_{\rm dof}}$  to lie within  $\pm 2$  of zero 95 per cent of the time. This quantity is printed in Table 1 and shows that the recovered parameter values are indeed a good fit to the mock observations.

In each case, we see that the parameters are more precisely constrained as the axial ratio q decreases, and ellipticity increases, left to right. This is as expected, considering that the circular case provides no constraints on the mass profile. For Case 1, with  $\theta_T$  fixed, the expected anticorrelation between q and t is clearly seen i.e. as t increases, and the potential becomes more circular, this is compensated for by a decrease in q, or increase in ellipticity. For Case 2, where  $\theta_T$  is an extra free parameter, the main correlation is now between q and  $\theta_T$ : as  $\theta_T$  increases the potential becomes less circular, so q must increase, i.e. ellipticity must decrease, to compensate. Interestingly, the constraints on t are very similar for the same q, between Cases 1 and 2. We also created images with different values of  $\theta_T$  and confirmed that the constraints on t improve as  $\theta_T$  increases, as expected.

These results show that, although there is no mass in the annulus spanned by the images, the recovered values for the slope *t* are consistent with the input values. It is clear that for a non-circular lens, the images do provide a constraint on the interior mass profile. This constraint is found to improve with ellipticity, and as the truncation radius approaches the radius of the images. In the best case, constraints of  $\sigma_t < 0.05$  can be achieved on the interior slope. In Section 1, we drew attention to a belief frequently found in the literature that lensing measures the slope of the profile at the Einstein radius, and not interior to the images. The results presented here contradict this belief.

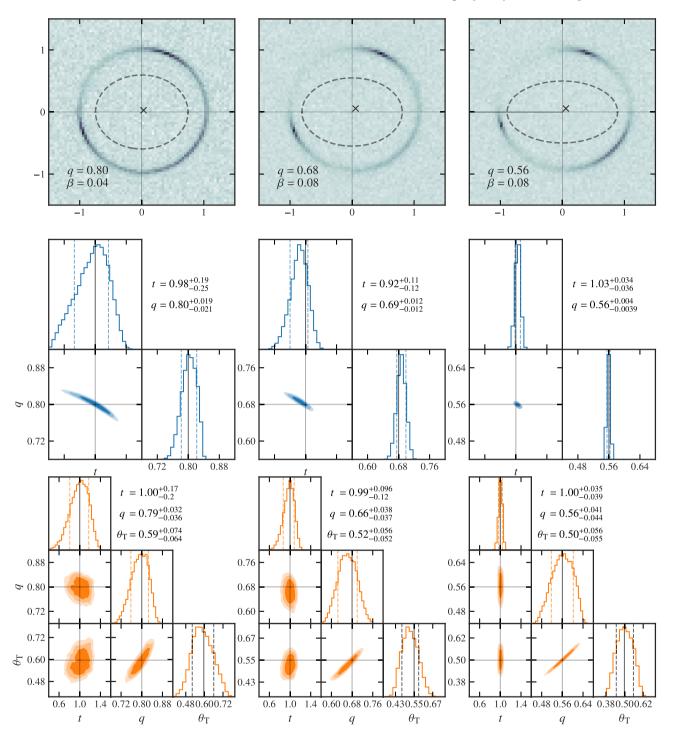
### 6 SUMMARY

In this paper, we have derived the lensing properties of the 2DBPL model, a versatile model for determining the projected mass profile of the lens, comprising power laws of slope  $t_1$  and  $t_2$  either side of the break radius  $\theta_B$ . This model is the simplest extension of the power law traditionally used in lensing studies, adding two degrees of freedom. We also presented a method for the efficient computation of the BPL model.

The BPL model derives from the TPL model. In the TPL model, the surface density is described by a power law inside some elliptical radius, called the truncation radius, and is zero outside. Using mock observations constructed with the TPL model, we showed that, for an elliptical lens, the observations can constrain the slope interior to the images. The ellipticity of the lens and the truncation radius are also measurable. The sensitivity to the slope interior to the images improves with increasing ellipticity. This result contradicts the standard picture that lensing measures the slope of the mass profile at the Einstein radius and is insensitive to the mass profile interior to the images.

This demonstration opens up the possibility of using strong gravitational lensing to analyse the projected mass profile in detail. In the next paper, we will present a full exploration of the usefulness of the BPL model for measuring mass profiles in lens galaxies. We will determine the uncertainties on the parameters  $t_1$ ,  $t_2$ , and  $\theta_B$ 

<sup>&</sup>lt;sup>1</sup>The infinite width of the Sérsic profile means there is actually a vanishingly small amount of source flux inside the truncation radius. In the mock observation with an image closest to the truncation radius (the third observation in Fig. 4), the ratio of source flux inside  $\theta_T$  to the total flux is 0.002. In general, the source flux interior to  $\theta_T$  is well below the average noise level and will not contribute to the fit.



**Figure 4.** Constraints on the mass profile slope *t*, axial ratio *q*, and break radius  $\theta_T$  for three truncated systems, created with signal-to-noise ratio S = 100. *Top row:* Image plane. The dashed ellipse marks the truncation radius and the cross is the source position. *Middle row:* Case 1 results,  $\theta_T$  fixed. *Bottom row:* Case 2 results,  $\theta_T$  free. Contours are the 68 per cent, 95 per cent, and 99 per cent credible intervals. The 68 per cent credible intervals are also shown as dashed lines in the 1D histograms. Solid grey lines in the histograms mark the true values.

over the parameter space of source position and lens ellipticity. This identifies the particular configurations where all three parameters may be measured accurately, which are the most useful for detailed study, for example, in measuring the Hubble constant.

# ACKNOWLEDGEMENTS

We are grateful to the Imperial College Research Computing Service for HPC resources and support. CMO'R is supported by a Science and Technology Facilities Council (STFC) Studentship. **Table 1.** Goodness of fit for the recovered parameter values in the three systems in Fig. 4, ordered left to right. These values are for the full 12 parameter fit, i.e. those including  $\theta_{\rm T}$  as a parameter.  $\chi^2$  is calculated in a mask surrounding the images (see Paper I, section 3.3). The number of degrees of freedom,  $N_{\rm dof}$ , is the number of pixels in the mask minus the number of fitted parameters.

System	$\chi^2$	$N_{ m dof}$	$\frac{\chi^2 - N_{\rm dof}}{\sqrt{2N_{\rm dof}}}$
1	533.76	573	- 1.16
2	598.36	541	1.74
3	529.89	485	1.44

# DATA AVAILABILITY

The data used in this paper are available from the corresponding author on request.

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