# **Optical and spectral observations and hydrodynamic modelling of type IIb supernova 2017gpn**

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## ABSTRACT

In this work we present the photometric and spectroscopic observations of type IIb supernova 2017gpn. This supernova was discovered in the error-box of the LIGO/Virgo G299232 gravitational-wave event. We obtained the light curves in the *B* and *R* passbands and modelled them numerically using the one-dimensional radiation hydrocode STELLA. The best-fitting model has the following parameters: the pre-SN star mass and the radius are  $M \approx 3.5 \text{ M}_{\odot}$  and  $R \approx 50 \text{ R}_{\odot}$ , respectively; the explosion energy is  $E_{\text{exp}} \approx 1.2 \times 10^{51}$  erg; the mass of radioactive nickel is  $M_{56}_{\text{Ni}} \approx 0.11 \text{ M}_{\odot}$ , which is completely mixed throughout the ejecta; and the mass of the hydrogen envelope  $M_{\text{H},\text{env}} \approx 0.06 \text{ M}_{\odot}$ . Moreover, SN 2017gpn is a confirmed SN IIb that is located at the farthest distance from the centre of its host galaxy NGC 1343 (i.e. the projected distance is ~21 kpc). This challenges the scenario of the origin of type IIb supernovae from massive stars.

Key words: supernovae: general – supernovae: individual: SN 2017gpn – stars: evolution.

## **1 INTRODUCTION**

Type IIb supernovae (SNe IIb) are characterized by spectra evolving from dominant hydrogen lines at early times to increasingly strong helium features and progressively weaker hydrogen lines later on (Filippenko, Matheson & Ho 1993). This is the reason why SNe IIb are regarded as an intermediate group between hydrogenrich SNe II and hydrogen-poor SNe Ib. SNe IIb are in the class of the stripped-envelope core-collapse supernovae (CCSNe). It is supposed that progenitors of such supernovae are massive stars that have lost most of their hydrogen envelope (Clocchiatti & Wheeler 1997).

Nowadays there are two hypotheses explaining how stars can lose the hydrogen envelope. The first scenario supposes the evolution of a rather massive  $M \simeq 25 \,\mathrm{M_{\odot}}$  single star with an average mass-loss rate of about  $10^{-5} \,\mathrm{M_{\odot}} \,\mathrm{yr^{-1}}$ . Such a powerful stellar wind could provide the required outflow of hydrogen (Hoflich, Langer & Duschinger 1993). The second and more plausible scenario involves a mass transfer in a binary system where the progenitor star is a supergiant of moderate mass (Nomoto et al. 1993; Woosley et al. 1994; Ergon et al. 2015). The massive companion expands and fills its Roche lobe, after which mass transfer starts due to Roche-lobe overflow (Yoon, Dessart & Clocchiatti 2017). Nevertheless, the progenitor nature of SNe IIb is still not clear. While SNe II form a continuous group as Anderson et al. (2014) and Sanders et al. (2015) established, Pessi et al. (2019) showed that SN II light curves are distinct from those of SNe IIb with no suggestion of a continuum distribution. This fact suggests that progenitors of SNe IIb make up a separate group that is different from the SNe II ones. However, it could also be a consequence of the lack of observational data: SNe IIb make up less than 5 per cent of all CCSNe according to the Open Supernova Catalog<sup>1</sup> (Guillochon et al. 2017) and only about two dozen of them have detailed multicolour photometry appropriate for further study (including hydrodynamic modelling).

To extend the sample of well-studied SNe IIb, in this paper we present the photometric and spectroscopic observations of SN 2017gpn. The photometry was performed with the Zeiss-1000 telescope (Komarov et al. 2020) at the Special Astrophysical Observatory of the Russian Academy of Science (SAO RAS). Spectroscopic data were obtained with the Xinglong 2.16-m telescope at the National Astronomical Observatory of China. Collected photometric data are used for the numerical light-curve (LC) calculations done by the radiation hydrocode STELLA (Blinnikov et al. 1998, 2006). These simulations give us the parameters of the pre-supernova star and explosion characteristics.

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The interest in this supernova is also augmented by the fact that we usually only observe such supernovae in spiral galaxies in hydrogen-rich environments where young massive stars are being born (Filippenko 1997). In contrast to this, SN 2017gpn is located quite far from the active star-formation regions and the spiral arms of the host galaxy. We also do not see any dwarf satellite galaxies at the SN location. The unusual location of SN 2017gpn in the host galaxy indicates that the existing models of SN IIb progenitors may not explain all observational data and have to be reviewed.

This paper is organized as follows. In Section 2 we describe the observations, data processing, and resulting light curves and spectra. In Section 3 we present the hydrodynamic modelling of SN 2017gpn and the parameters of the best-fitting model. Section 4 contains a comparison of the modelling results, LC behaviour, and spectral features of SN 2017gpn with those for other SNe IIb and a discussion of the unexpected location of SN 2017gpn relative to its host galaxy. Finally, we conclude the paper in Section 5.

## 2 OBSERVATIONS

#### 2.1 Discovery

On the last day of the second advanced detector observing run 'O2', the LIGO/Virgo Collaboration released the G299232 alert.<sup>2</sup> During the follow-up inspection of the gravitational-wave (GW) candidate error-box, on 2017 August 27.017 the MASTER Global Robotic Net (Lipunov et al. 2010) discovered an optical transient named MASTER OT J033744.97+723159.0 (Lipunov et al. 2017).

On the discovery day, three spectra of MASTER OT J033744.97+723159.0 were obtained with the ACAM instrument mounted on the William Herschel Telescope at La Palma (Spain) by Jonker et al. (2017) and the analysis showed that the transient classifies as SNe IIb. Further observations on 2017 August 29 obtained with the SPRAT spectrograph on the Liverpool Telescope (Copperwheat et al. 2017) and with the Xinglong 2.16-m telescope of the National Astronomical Observatory of China (Rui et al. 2017; Wang 2017) confirmed this classification by cross-correlating with a library of spectra with use of the Supernova Identification code (SNID; Blondin & Tonry 2007). According to SNID, the spectrum with the highest correlation coefficient belongs to type IIb SN 1996cb at phase -2 d.

On 2017 September 6 at 03:21:12 UT, Caimmi (2017) reported the discovery of a supernova with the 0.24-m telescope from the Valdicerro Observatory. The supernova received the IAU designation AT 2017gpn and was identified as MASTER OT J033744.97+723159.0.

SN 2017gpn is located ~140 arcsec from the centre of the host galaxy NGC 1343 (Fig. 1). Taking into account that the redshift of NGC 1343 is 0.0073 (Springob et al. 2005) and assuming flat  $\Lambda$ CDM cosmology with  $\Omega_{\Lambda} = 0.7$  and  $H_0 = 70$  km s<sup>-1</sup> Mpc<sup>-1</sup>, we find that the projected distance between SN 2017gpn and the centre of its host is ~21 kpc.

#### 2.2 Photometric data processing

We performed 20 epochs of observations (B and R passbands) with the CCD photometer on the Zeiss-1000 telescope at SAO RAS. The aperture photometry was performed using standard procedures of the ESO MIDAS software package. It includes standard image processing

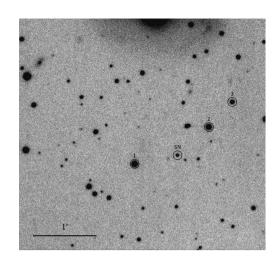


Figure 1. SN 2017gpn and comparison stars. The image is obtained with the Zeiss-1000 telescope in the *R* passband.

**Table 1.** Magnitudes of the comparison stars in the *B* and *R* passbands derived from *g*, *r*, *i* Pan-STARRS 1 magnitudes using Lupton's 2005 transformation equations.

N⁰	В	err <sub>B</sub>	R	err <sub>R</sub>
1	16.447	0.011	15.032	0.015
2	16.859	0.012	15.428	0.015
3	17.705	0.011	16.636	0.017

such as bias subtraction and flat-field correction, removing the traces of cosmic particles, and stacking of individual frames into a summary image.

Since no Landolt or any other standards (Stetson 1987; Landolt 1992) were available for this region, we use the Pan-STARRS (Chambers et al. 2016; Flewelling et al. 2016) magnitudes for comparison stars. These magnitudes were recalculated from the *g*, *r*, *i* passbands to *B* and *R* with the use of Lupton's transformation equations<sup>3</sup>:

$B = g + 0.3130 (g - r) + 0.2271, \ \sigma = 0.0107$	
$R = r - 0.1837 \left(g - r\right) - 0.0971, \ \sigma = 0.0106$	
$R = r - 0.2936 (r - i) - 0.1439, \sigma = 0.0072.$	(1)

The comparison stars are shown in Fig. 1 and their magnitudes are listed in Table 1.

We use a line-of-sight reddening for the Galaxy of E(B - V) = 0.30 mag (Schlafly & Finkbeiner 2011), corresponding to additive magnitude corrections of 1.246 and 0.725 mag for the *B* and *R* passbands, respectively. Since SN 2017gpn is very far from the centre of NGC 1343, we assume that the host's contamination is negligible. The resulting photometric data are presented in Table 2.

#### 2.3 Resulting light curves

With the Zeiss-1000 observations we can restore only the postmaximum part of the light curve. This is why, to improve the accuracy of the further hydrodynamic modelling (see Section 3), we supplemented our data with observations in the *B* and *R* passbands from Roberts & Kolb (2018) obtained with the PIRATE robotic telescope in Spain (Holmes et al. 2011). The resulting light curve is

 Table 2. Photometric observations of SN 2017gpn with the Zeiss-1000 telescope. The magnitudes are corrected for the expected Galactic foreground extinction.

JD 245 7990 +	В	err <sub>B</sub>	R	err <sub>R</sub>
21.5	16.65	0.07	15.34	0.03
22.5	16.75	0.05	15.41	0.02
25.6	17.08	0.05	15.58	0.03
26.5	17.16	0.05	15.62	0.04
27.5	17.24	0.06	15.67	0.02
28.5	17.33	0.06	15.73	0.02
29.6	17.35	0.05	15.81	0.02
31.5	17.44	0.06	15.88	0.03
56.4	17.90	0.06	16.62	0.02
57.4	17.89	0.05	16.63	0.01
76.5	_	_	17.17	0.03
77.4	18.17	0.07	17.13	0.03
78.6	18.14	0.06	17.21	0.03
85.6	18.22	0.05	17.21	0.03
107.6	_	_	18.06	0.04
110.4	18.61	0.07	17.89	0.03
143.3	19.14	0.15	18.78	0.01
153.3	_	_	18.54	0.30
224.3	-	-	21.14	0.20

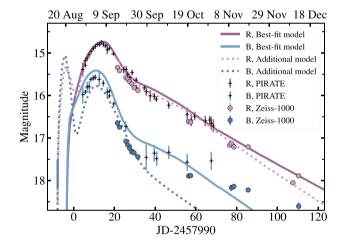


Figure 2. Light curve of SN 2017gpn. Pink and blue solid lines correspond to the best-fitting model; dashed lines, to the additional model in the R and B passbands, respectively. Circles are the Zeiss-1000 data; crosses are the data taken from Roberts & Kolb (2018).

presented in Fig. 2. The data points obtained at Zeiss-1000 (shown as circles) and the data points taken from Roberts & Kolb (2018) (marked with crosses) mutually complement each other and allow us to restore the *B* and *R* light curves almost entirely.

One can notice a slight shift between the two data sets. This may be due to the different sources of photometry for the comparison stars since there are no Stetson and Landolt photometric standards in this field. However, the difference between the values is less than the uncertainty associated with the choice of hydrodynamic model; therefore for our purpose it can be neglected.

#### 2.4 Spectra

The spectroscopic observations were collected using the Xinglong 2.16-m telescope and the BFOSC system. All the spectra were reduced using routine tasks within IRAF and the flux was calibrated

with spectrophotometric standard stars observed on the same nights. Telluric lines are removed from all of these spectra. The journal of our spectroscopic observations is given in Table 3.

Three optical spectra were obtained for SN 2017gpn, covering the phases from -8.3 to +19.7 d from the *R*-band maximum light (peak time is  $JD = 245\,8003.6$ ); these are shown in Fig. 3. At one week before the peak, the spectrum shows strong Balmer lines of hydrogen, providing evidence of a type II supernova. Moreover, the existing prominent absorption features at  $\sim$ 5670 and 6860 ÅÅ that can be identified as HeI  $\lambda$ 5876 and HeI  $\lambda$ 7065, respectively, confirming that SN 2017gpn can be further put into the type IIb subclass. From the absorption minima of H  $\alpha$  and He I  $\lambda$ 5876 lines at the first obtained spectrum, we measured the ejecta velocity as  $15\,000 \pm 130$  and  $10\,100 \pm 300$  km s<sup>-1</sup>, respectively, indicating that the Balmer lines and the HeI lines originated from different layers (see Table 3). At two weeks after the maximum, the helium features seem to become more noticeable and other helium features such as He I  $\lambda$ 6678 (blueshifted to ~6510 Å) emerge in the spectrum. The helium features become even more pronounced in the spectrum taken one week later, while the hydrogen features become gradually weaker. The overall spectral evolution of SN 2017gpn is presented in Fig. 3 and it is similar to other typical type IIb supernovae, like SN 1993J (Barbon et al. 1995), SN 1996cb (Qiu et al. 1999), and SN 2008ax (Modjaz et al. 2014).

#### **3 MODELLING**

#### 3.1 Pre-supernova models

A set of non-evolutionary pre-supernova models is obtained under the assumption of a power-law dependence of temperature on density:  $T \propto \rho^{\alpha}$  (Nadyozhin & Razinkova 1986; Blinnikov & Bartunov 1993). Therefore, the obtained hydrostatic configuration would be close to a polytrope of index  $1/\alpha \simeq 3$ . The deviation from the polytropic model increases in the outer layers due to recombination of ions and non-homogeneous chemical composition.

At the centre of such a configuration we isolated a point-like source of gravity that has a non-negligible influence on the expansion of the innermost layers of supernova ejecta. The mass and radius of this compact remnant are taken as  $M_{\rm CR} = 1.41 \text{ M}_{\odot}$  and 0.01 R<sub> $\odot$ </sub> for all treated pre-SN models.

In our approach we do not follow the explosive nucleosynthesis. Thus, the SN ejecta composition is the same as the pre-SN composition except for <sup>56</sup>Ni. Since the amount and distribution of <sup>56</sup>Ni synthesized during the explosion plays a crucial role in the SN luminosity evolution, we consider two radial distributions for <sup>56</sup>Ni. In the first one <sup>56</sup>Ni is totally mixed through the ejecta and in the second one <sup>56</sup>Ni falls off from the centre.

As input parameters for further hydrodynamical modelling, we varied the pre-SN star mass M and the radius R, the mass of synthesized nickel  $M_{56_{\text{Ni}}}$ , and the initial distribution of chemical elements in the pre-SN star.

## 3.2 STELLA code

To explode the hydrostatic non-evolutionary pre-SN models a onedimensional multifrequency radiation hydrocode STELLA is used. The full description of the code can be found in Blinnikov et al. (1998, 2006); a public version of STELLA is also included with the MESA distribution (Paxton et al. 2018). The STELLA code is used for the light-curve modelling of different types of SNe – Ia (Blinnikov et al. 2006), Ib/Ic (Folatelli et al. 2006; Tauris et al.

**Table 3.** Journal of spectroscopic observations of SN 2017gpn with the BFOSC + G4 instrument of the Xinglong 2.16-m telescope. Values of the ejecta velocity measured from the absorption lines of H $\alpha$ , He I  $\lambda$ 5876, Fe II  $\lambda$ 5018, and Fe II  $\lambda$ 5169 are also presented.

JD 245 7990 +	Exp. time [s]	$H\alpha$ [km s <sup>-1</sup> ]	He I $\lambda$ 5876 [km s <sup>-1</sup> ]	Fe II λ5018 [km s <sup>-1</sup> ]	Fe II λ5169 [km s <sup>-1</sup> ]
5.30	3600	$15000\pm130$	$10100\pm300$	$12000\pm1200$	$11400\pm950$
25.29	3600	$13200\pm100$	$8000\pm100$	$6750 \pm 470$	$5130\pm490$
33.33	2700	$12900\pm200$	$7300\pm200$	_	-

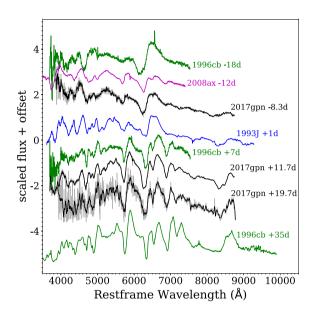


Figure 3. Three spectra of SN 2017gpn at different phases; the observation dates are indicated with respect to the *R*-band maximum light at  $JD = 245\,8003.6$ . Spectra of SNe IIb 1993J, 1996cb, and 2008ax are presented for comparison.

2013), IIb (Blinnikov et al. 1998; Tsvetkov et al. 2012), IIn (Chugai et al. 2004), IIP (Baklanov, Blinnikov & Pavlyuk 2005; Tominaga et al. 2009), Ic associated with long gamma-ray bursts (Volnova et al. 2017). The STELLA code was compared with other well-known hydrodynamic codes and found to be in good agreement with them on the level of several per cent (e.g. Woosley et al. 2007; Kromer & Sim 2009; Sim et al. 2010; Kozyreva et al. 2017; Tsang et al. 2020).

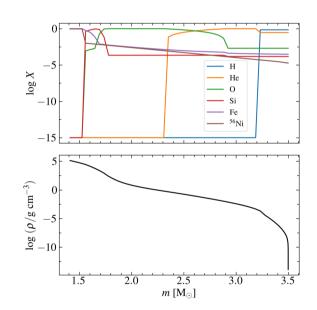
In the current calculations, we adopted 100 zones for the Lagrangian coordinate and 130 frequency bins. The explosion is initiated by putting thermal energy into the innermost layers. The energy is released in 0.1 s, which is less than the hydrodynamic time of the pre-supernova. While this condition is true, the resulting light curve is not affected by the details of the explosion mechanism (Imshennik & Nadezhin 1983).

#### 3.3 Best-fitting model

To determine the best-fitting model of SN 2017gpn we consider a grid of parameters. The pre-SN mass varies between 3.5 and 5.5  $M_{\odot}$  with steps of 0.5  $M_{\odot}$ ; the pre-SN radius and  $E_{exp}$  take the values {50, 100, 200, 400, 600}  $R_{\odot}$  and {0.6, 1.2, 2.4} × 10<sup>51</sup> erg, respectively; three different  $M_{56}_{Ni}$  {0.07, 0.09, 0.11}  $M_{\odot}$  are considered, both with and without mixing. The mass of the hydrogen envelope  $M_{H.env}$  is taken as 0.06  $M_{\odot}$ , which is in line with our expectations for type IIb supernovae.

**Table 4.** Parameters for the best-fitting and additional hydrodynamic modelsof SN 2017gpn.

Parameter	Best-fitting model	Additional model
R	$50 \ R_{\odot}$	$400~R_{\odot}$
М	3.5 M <sub>☉</sub>	3.5 M <sub>☉</sub>
$M_{\rm H_{env}}$	$0.06 \ \mathrm{M_{\odot}}$	0.21 M <sub>☉</sub>
M <sub>CR</sub>	1.41 M <sub>☉</sub>	1.41 M <sub>☉</sub>
$M_{56\rm Ni}$	$0.11 \text{ M}_{\odot}$ , mixed	$0.11 \text{ M}_{\odot}$ , no mixing
$E_{\rm exp}$	$1.2 \times 10^{51} \text{ erg}$	$1.2 \times 10^{51} \text{ erg}$
t <sub>peak,R</sub>	2017 Sept 7.5	2017 Sept 5.6



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Figure 4. Mass fractions of the most abundant chemical elements in the ejecta (top) and density profile (bottom) for the best-fitting pre-SN star model with respect to the interior mass. The central region of  $1.41 M_{\odot}$  is taken away.

After determination of the parameter grid we built trial models and chose the best-fitting model within the generated grids of light curves by calculating  $\chi^2$  in the *R* passband. The best-fitting model corresponds to the minimum value of  $\chi^2$ . We do not provide any statistical uncertainties, since this procedure requires enormous computational effort. Instead, the optimal model is recovered as a compromise between the fits to the observed light curve and the evolution of the velocity at the photosphere (see Section 4.2.1). The values of the best-fitting model parameters are summarized in Table 4. Fig. 2 compares the light curves of the model (solid lines) with the observations of SN 2017gpn.

In Fig. 4 we also show the distribution of the chemical elements and the density profile for a pre-SN star. Note that the best-fitting model shows a small amount of hydrogen in the pre-SN star composition,

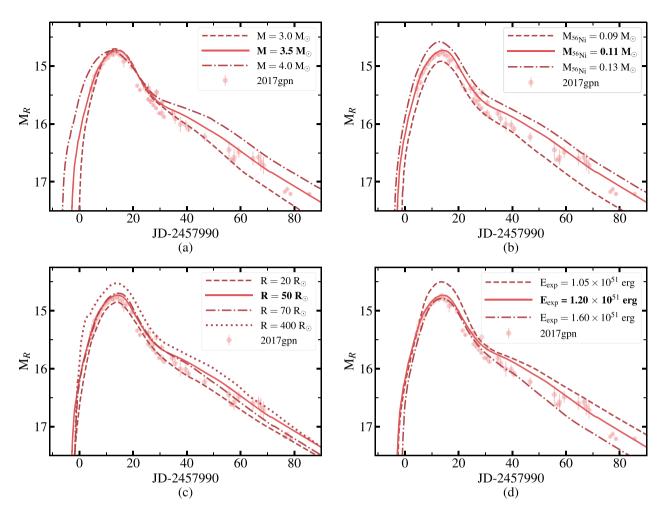


Figure 5. The dependence of the modelled *R*-passband LC on the pre-SN mass *M* (a), the amount of synthesized <sup>56</sup>Ni (b), the pre-SN radius *R* (c), and the explosion energy  $E_{exp}$  (d). All models are shifted along the time axis to better describe the observations. The best-fitting model is shown by a solid line in all plots; observations are shown by circles.

which is expected for SNe IIb (Filippenko et al. 1993). <sup>56</sup>Ni is totally mixed through the ejecta.

#### 3.4 The influence of the model parameters on the light curve

To provide a reasonable range of the best-fitting model parameters, we consider the dependence of the numerical LCs on an input parameter of the model while the others remain fixed. We vary the mass M and the radius R of the pre-SN star, the mass of synthesized <sup>56</sup>Ni, and the energy of the explosion  $E_{exp}$ . In Fig. 5 we plot some modelled LCs in the R passband that show a valid range for each parameter. All presented models are slightly shifted along the time axis to better describe the observational light curve.

The first considered parameter is the pre-SN mass *M*; see Fig. 5(a). This parameter mainly affects the width of the light curve, which becomes broader as the mass increases. This is explained by the fact that with a small mass the envelope becomes transparent faster. Thus, the LC increases before the maximum light and decreases rapidly after it. As Fig. 5(a) shows, the range of valid pre-SN mass is  $3-4 \text{ M}_{\odot}$ .

The next parameter is the amount of synthesized <sup>56</sup>Ni (Fig. 5b). The models are brighter for higher <sup>56</sup>Ni masses. The LCs corresponding to the <sup>56</sup>Ni masses of 0.09 and 0.13  $M_{\odot}$  lie below and above the

best-fitting model light curve, respectively. These two values define the acceptance range of the  $M_{56Ni}$  model parameter.

The pre-SN radius affects mainly the light-curve tail: a larger radius value corresponds to a brighter light curve after maximum light. The chosen range of the pre-SN radius is 20–70  $R_{\odot}$ ; see Fig. 5(c).

The last parameter that we vary is the explosion energy  $E_{\rm exp}$ ; see Fig. 5(d). The determined range for the energy parameter is  $(1.05-1.60) \times 10^{51}$  erg. As seen from Fig. 5(d), smaller values of  $E_{\rm exp}$  correspond to brighter light curves. This dependence is in line with our expectations. A larger  $E_{\rm exp}$ , for a fixed mass of <sup>56</sup>Ni and fixed total mass, implies higher velocities and hence less trapping of gamma-ray photons. This leads to an increase in the predicted observed gamma-ray flux and, therefore, to a decrease in the emission in the visible light range.

### **4 DISCUSSION**

#### 4.1 Comparison with other SNe IIb

We collected data for well-studied SNe IIb with good photometric coverage in the B and R passbands, for which results of hydrodynamic modelling can be found in the literature. In Fig. 6 the light curves of

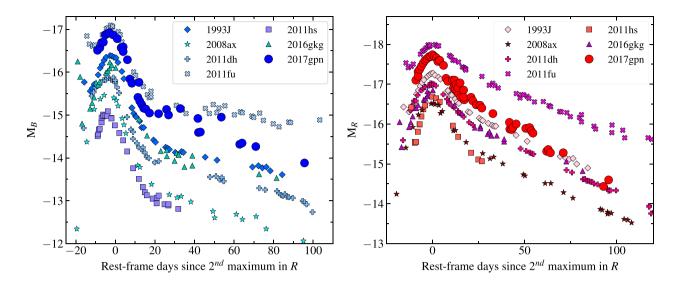


Figure 6.  $M_B$  and  $M_R$  light curves of SN 2017gpn in comparison with those of other type IIb supernovae: 1993J (Richmond et al. 1996), 2008ax (Tsvetkov et al. 2009), 2011dh (Tsvetkov et al. 2012), 2011fu (Kumar et al. 2013), 2011hs (Bufano et al. 2014), 2016gkg (Bersten et al. 2018).

selected SNe IIb are presented. It can be seen that LCs in the *B* and *R* passbands are similar – characteristic bell-shaped LCs. Moreover, as Pessi et al. (2019) showed, SNe IIb take longer to reach maximum light and decline more quickly post-maximum than hydrogen-rich SNe II, so the authors assume that there is no continuum between SNe IIb and other SNe II like between SNe IIP and IIL types. SN 2017gpn has a typical SN IIb light curve, and belongs to one of the brightest well-studied SNe IIb: it is brighter than a typical member of type IIb SN 1993J by 0.75 mag in the *R* passband.

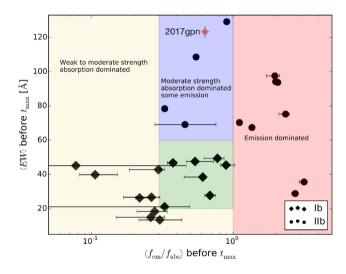
## 4.1.1 Classification of Prentice & Mazzali (2017)

Following Prentice & Mazzali (2017), stripped-envelope SNe should be subclassified into four groups: Ib, Ib(II), IIb, and IIb(I), using the additional parameters – equivalent width of H $\alpha$  (EW<sub>H $\alpha$ </sub>) and H $\alpha$  emission-to-absorption ratio  $f_{\rm em}/f_{\rm abs}$ . The EW<sub>H $\alpha$ </sub> parameter value is >60Å for supernovae of group IIb(I), 20 < EW<sub>H $\alpha$ </sub> < 60Å for Ib(II), and takes any reasonable value for groups Ib and IIb. The H $\alpha$  emission-to-absorption ratio  $f_{\rm em}/f_{\rm abs}$  differs for groups IIb and IIb(I): it ranges from 0.3–1 for IIb(I) and is greater than 1 for group IIb (see Fig. 7).

We calculated the intensity and equivalent width of H $\alpha$  in our first spectrum (-8.3 d before *R*-band maximum) for SN 2017gpn and found  $f_{\rm em}/f_{\rm abs} = 0.63 \pm 0.04$ , EW<sub>H $\alpha</sub> = 123 \pm 3$  Å. Therefore, SN 2017gpn belongs to group IIb(I), which means that it might have less hydrogen in the envelope than most H-rich SNe such as 1993J, 2011fu, or 2011dh (see Table 5). However, it is similar to other SNe IIb(I) – 2008ax and 1996cb (the first position in a cross-correlation list according to SNID).</sub>

#### 4.1.2 Hydrodynamic models of other SNe IIb

We compare the results of numerical simulations for SN 2017gpn and other SNe IIb (including groups IIb and IIb(I) of Prentice & Mazzali 2017) presented in Fig. 6. Only hydrodynamic modelling of supernovae is chosen for comparison; we do not consider any analytical light-curve modelling or scaling to templates. The modelling results are summarized in Table 5, where  $M_{CR}$  is the mass of a



**Figure 7.** This figure is borrowed from Prentice & Mazzali 2017 (fig. 7) with SN 2017gpn plotted (pink square). It illustrates the stripped-envelope supernovae subclassification based on the comparison of the line strength (equivalent width of H  $\alpha$ ) against the line profile (H  $\alpha$  emission-to-absorption ratio  $f_{em}/f_{abs}$ ) as proposed by Prentice & Mazzali (2017). SN 2017gpn lies in the blue region that corresponds to group IIb(I). Groups IIb, Ib, and Ib(II) are in the red, yellow, and green regions, respectively.

compact object (generally this is a neutron star) and  $M_{\rm ej}$  is the mass of ejected matter.

The main modelling parameters such as the ejecta mass  $M_{\rm ej}$ , the mass of <sup>56</sup>Ni,  $M_{\rm H,env}$ , and the explosion energy  $E_{\rm exp}$  are consistent with each other. An exception is the parameter of the pre-supernova radius R. The considered hydrodynamic modelling shows that the pre-SN radius lies in a broad range from 30–720 R<sub> $\odot$ </sub> and may be different for the same object in different models. For example, there are two models for SN 2008ax, one with a radius of 30–50 R<sub> $\odot$ </sub> (Folatelli et al. 2015) and another one with  $R = 600 R_{\odot}$  (Tsvetkov et al. 2009). It should be noted that SN 2008ax belongs to the same group of IIb(I) supernovae as SN 2017gpn.

SN name	$M_{ m CR}$ [M $_{\odot}$ ]	$M_{ m ej}$ $[{ m M}_{\odot}]$	$M_{ m 56Ni}$ $[{ m M}_{\odot}]$	$M_{ m H\_env}$ [M $_{\odot}$ ]	<i>R</i> [R <sub>☉</sub> ]	$E_{exp}$ [10 <sup>51</sup> erg]	Reference
1993J	~1.4	1.4–3.1	0.06-0.08	0.2	430–720	1.2	Woosley et al. (1994) Blinnikov et al. (1998)
2008ax	1.41	2.39	0.11	_	600	1.5	Tsvetkov et al. (2009)
2008ax	1.5	1.8-3.5	0.05 - 0.07	0.06	30-50	0.8 - 1.2	Folatelli et al. (2015)
2011hs	1.5	1.5-2.5	0.04	< 0.5	500-600	0.85	Bufano et al. (2014)
2011fu	1.5	3.5	0.15	0.3	450	1.3	Morales-Garoffolo et al. (2015)
2011dh	1.41	2.24-4.24	0.07	_	150-300	2–4	Tsvetkov et al. (2012)
2011dh	1.5	2	0.06	0.1	200	0.6-1	Bersten et al. (2012)
2011dh	1.5	1.56	0.075	0.1	200-300	0.58	Ergon et al. (2015)
2016gkg	1.4	3.55	0.2	0.02	180-260	1.3	Piro et al. (2017)
2016gkg	1.5-1.6	2.5-3.4	0.085 - 0.087	0.01-0.09	300-340	1 - 1.2	Bersten et al. (2018)

Table 5. Comparison of the hydrodynamic modelling results for different SNe IIb.

## 4.2 Additional model

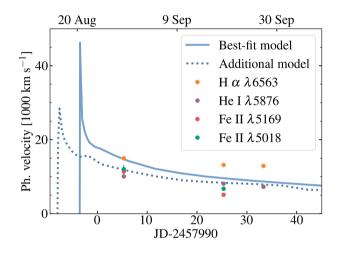
Motivated by the discrepancy in the modelled radius for different SNe IIb, we have found another physically reasonable model for SN 2017gpn with  $R = 400 \text{ R}_{\odot}$ . For this additional model, radioactive nickel is located in the central part of the ejecta. We have also increased the mass of the hydrogen envelope to 0.21 M<sub> $\odot$ </sub>, which is consistent with the fact that more extended SNe IIb should be also more H-rich (Prentice & Mazzali 2017). The parameters of the additional model are listed in Table 4. This model also well describes the observational data and agrees with the results of the hydrodynamic simulations for other SNe IIb.

There is no direct method to solve the inverse problem, i.e. to determine the parameters of the pre-supernova from the observational data. We can only build a model with given parameters and see how accurately it fits the data. Sometimes it can happen that models with different parameters reproduce observations equally well, as we see for our best-fitting and additional models (Fig. 2). However, if some additional information is available, e.g. observational photospheric velocities, we can compare our theoretical estimations with the observational values and make a choice between the models.

#### 4.2.1 Photospheric velocities

Based on three spectra of SN 2017gpn obtained at different epochs with the Xinglong 2.16-m telescope, we measured the ejecta velocity from the H $\alpha$  and He I  $\lambda$ 5876 absorption lines (Table 3). In Fig. 8 we show the comparison between the velocities measured from these lines and theoretical values from the STELLA code, which are the velocities of the photosphere at the  $\tau = 2/3$  level in the *B* band. The best-fitting model is consistent with the velocity measured from the H $\alpha$  line for this epoch; the additional model is in good agreement with the He I  $\lambda$ 5876 velocities for all three epochs.

It should be noted that P Cygni profiles are formed in all layers above the photosphere. Hence, the hydrogen and helium features do not necessarily reflect the photospheric velocities calculated by our hydrodynamic modelling. It has to be taken into account that the growth of the Sobolev optical depth (Sobolev 1960) at the photosphere level causes a significant blueshift of the P Cygni profile minimum, so the resulting velocity in that case will be overestimated (Kasen et al. 2002). This effect may explain why the velocities measured from the H  $\alpha$  line are greater than our theoretical estimates in Fig. 8. Meanwhile, according to Dessart & Hillier (2005, 2006) the velocities measured from strong lines can be both smaller and larger than the photospheric ones.



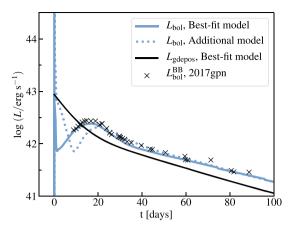
**Figure 8.** Photospheric velocity at the  $\tau = 2/3$  level as a function of time for the best-fitting model (solid line) and for the additional model of higher radius (dashed line); dots are the observational velocities measured from the H  $\alpha$ , He I  $\lambda$ 5876, Fe II  $\lambda$ 5018, and Fe II  $\lambda$ 5169 absorption lines.

Therefore, it is more reasonable to use 'weak' lines, i.e. lines with small Sobolev optical depths, to estimate  $v_{\rm ph}$ . Dessart & Hillier (2005) show that Na ID, Fe II  $\lambda$ 5018, Fe II  $\lambda$ 5169 are the most suitable lines to measure the photospheric velocities. We measured the velocities from the Fe II  $\lambda\lambda$ 5018 and 5169 lines for the first and second epochs of observations; the last epoch spectrum has a low signal-to-noise ratio to perform the measurements. We could not determine the velocities using Na ID features since they are close to the He I  $\lambda$ 5876 line, which is quite strong in SNe IIb.

The photospheric velocities derived for the additional model correspond slightly better to the velocities from the Fe II  $\lambda\lambda$ 5018 and 5169 lines for the first epoch of observations. For the second epoch the measured velocities are lower than the STELLA values for both models. Taking into account the modelling uncertainties, it is difficult to choose between the models based on these measurements only.

#### 4.2.2 <sup>56</sup>Ni mixing

From the theoretical bolometric LCs (Fig. 9) as well as LCs in filters (Fig. 2) it can be noticed that the light curve corresponding to the model with the uniform distribution of nickel behaves differently from the light curve that conforms with the model where nickel is concentrated in the centre of the ejecta. This is due to the fact that



**Figure 9.** Theoretical bolometric light curves for the best-fitting (blue solid line) and the additional (blue dashed line) models of SN2017gpn. The crosses show the bolometric luminosity of SN 2017gpn calculated from *B* and *R* light curves with use of the SUPERBOL code (Nicholl 2018). The shift between the data and the best-fitting model is the same as in Fig. 2 but transformed to the rest frame. The black solid line is the power due to the gamma-ray deposition from <sup>56</sup>Ni and <sup>56</sup>Co decays for our best-fitting model. Accounting for the light traveltime correction,  $L_{gdepos}$  satisfies Arnett's law, going through the maximum of  $L_{bol}$ .

in the former case the radioactive decay energy contributes to the overall energy immediately after the explosion, whereas in the latter case we observe two peaks in the light curve. The primary peak is associated with the heating of the outer layers of the star by the shock wave that is created by the rebound of the freely falling inner layers from the collapsed core. After that the envelope expands, cools, and therefore becomes transparent. The second peak is associated with the luminescence of the inner layers heated by the radioactive decays of <sup>56</sup>Ni and its products. For the additional model we fit the observed LCs by the second peak. Because of this, the best-fitting and additional models are shifted relative to each other in Fig. 2. The influence of <sup>56</sup>Ni mixing on the LC behaviour is also seen if we compare the additional model with the model in Fig. 5(c) (dotted line) with  $R = 400 \text{ R}_{\odot}$  and <sup>56</sup>Ni totally mixed through the ejecta. Unlike the additional model, this model no longer describes the observations.

In Fig. 9 we also show the bolometric light curve of SN 2017gpn restored from the available photometry. To construct the bolometric light curve the SUPERBOL code is used (Nicholl 2018). To account for flux that is not covered by the observations, the blackbody extrapolation is applied. Even though we use only two passbands (*B* and *R*) the obtained bolometric LC agrees very well with our theoretical estimations.

#### 4.3 Arnett's law

Arnett's law (Arnett 1982) states that the energy released on the surface at maximum light is equal to the energy deposed by gammaray radiation. This law is commonly used to estimate the amount of nickel produced in the explosion when the total luminosity at peak is known (Branch 1992). We plot the theoretical bolometric light curve and the curve corresponding to gamma-ray deposition from <sup>56</sup>Ni and <sup>56</sup>Co decays for our best-fitting model to check this law. As we can see from Fig. 9, the law is quite well satisfied; however, the power from gamma-ray deposition does not go directly through the  $L_{bol}$ peak. This is explained by the fact that Arnett's law is not exact and in particular assumes an infinite speed of light. In the STELLA code the energy released in the centre will be 'seen' with a delay of R/c, where R is the radius of the expanding ejecta that changes with time and c is the speed of light. The observed difference increases towards the tail since the radius increases as well.

#### 4.4 SN 2017gpn position relative to the host galaxy centre

Supernova 2017gpn exploded in the spiral galaxy NGC 1343 at a projected distance of  $D \simeq 21$  kpc from its centre (see Fig. 1). Such a location is unusual for core-collapse supernovae, in particular for type IIb, since it is believed that stripped-envelope CCSNe are formed from very massive stars in star-formation regions of galaxies (see Audcent-Ross et al. 2019 and references therein). Assuming that SN 2017gpn belongs to the galactic disc, we can take into account the projection effect. The deprojected distance  $D_{dep}$  between the supernova and the host centre is calculated as

$$D_{\rm dep} = D\sqrt{\cos^2\alpha + \sin^2\alpha \sec^2 i},\tag{2}$$

where  $\alpha$  is the angle between the projected distance and the major axis of a galaxy and *i* is the disc inclination angle. According to HyperLEDA *i* equals 67.3 deg and the major axis position angle of NGC 1343 is 78.8 deg (Makarov et al. 2014). Using these values and the coordinates of SN 2017gpn and its host galaxy centre we can calculate the deprojected distance for SN 2017gpn, which is ~52 kpc. To understand how exceptional this position is, we study the absolute and relative separations between the supernova positions and their host galaxy centres for a sample of SNe IIb.

Hereafter, by the distance between a supernova and its host galaxy we mean the projection of the distance on to the picture plane, which is obviously smaller than the real distance. However, star-evolution theory predicts that CCSNe including SNe IIb mainly appear in the galactic planes of spiral galaxies, in regions of high star-formation rate. Therefore, we assume that the contribution of the projection on to the line of sight is relatively small and this underestimation of the distance does not significantly affect our analysis.

We collected 71 confirmed SNe IIb and 108 candidates for SNe IIb from the Open Supernova Catalog (Guillochon et al. 2017). The confirmed SNe IIb are supernovae for which multiple spectra have been obtained and a detailed spectral analysis has been performed. If only a spectrum is available (usually single spectroscopic confirmation following the astronomical telegram about the transient discovery) we consider a supernova as a SN IIb candidate.

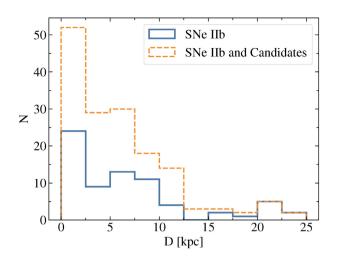
First, we calculated the absolute galactocentric distance *D* for each object as  $D \simeq d_a \times \Theta$ . The angle  $\Theta$  is the angle between the supernova and the host galaxy centre. The angular distance  $d_a$  for flat  $\Lambda$ CDM cosmology with  $\Omega_{\Lambda} = 0.7$  and  $H_0 = 70$  km s<sup>-1</sup> Mpc<sup>-1</sup> is

$$d_{\rm a} = \frac{c}{H_0 \times (1+z)} \int_0^z \frac{{\rm d}z'}{\sqrt{(1-\Omega_{\Lambda}) \times (1+z')^3 + \Omega_{\Lambda}}},\tag{3}$$

where z is the redshift and c is the speed of light. The distribution of type IIb supernovae by D is presented in Fig. 10. Most SNe IIb, about 85 per cent, are located inside a radius of 12 kpc. However, there is a local maximum near 20 kpc, which may be due to the fact that the radius of galaxies can vary widely.

To perform a more accurate analysis we determined the SN–host separation relative to the host size. To characterize the size of a galaxy we used a  $D_{25}$  value, which is the major diameter measured to the *B*-passband 25 mag arcsec<sup>-2</sup> isophote. The  $D_{25}$  values were extracted from the HyperLEDA extragalactic data base (Makarov et al. 2014).

The full list of studied supernovae and the absolute and relative distances are summarized in Table A1: the first column is the number



**Figure 10.** Histogram of the supernovae distribution depending on the projection of the distance between SN and its host galaxy centre, *D*. The orange dashed line corresponds to all considered supernovae including confirmed SNe IIb and candidates for SNe IIb. The solid blue line corresponds to the distribution of confirmed SNe IIb only.

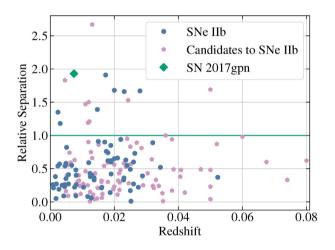


Figure 11. Relative separation between supernovae and their host galaxy centres as a function of redshift. Confirmed SNe IIb are plotted in blue dots; candidates for SNe IIb, in pink pentagons; and the studied SN 2017gpn is marked with the green diamond. SNe above the green line are considered to be distant from the centres of their hosts.

in the list for easier searching, the second column consists of the supernova names starting with confirmed SNe IIb, and continuing with SNe IIb candidates. The equatorial coordinates (RA, Dec.) of supernovae and their host galaxies are presented in the third, fourth, fifth, and sixth columns, respectively. The seventh column indicates the redshift *z*.  $D_{25}$  is given in column eight. The angle  $\Theta$  expressed in arcsec is shown in the ninth column. Columns 10 and 11 contain the absolute distance *D* in kpc and relative separation normalized to the size of the host galaxies, respectively.

In Fig. 11 we present the relative separation between SNe and their host galaxies depending on the redshift. To evaluate how far away a supernova is, we chose a value of 1 for the relative separation, which is shown by the horizontal green line in Fig. 11. There are eight SNe IIb that lie above the solid green line; we collect them into a group of distant supernovae. SN 2017gpn is the most distant from the host galaxy centre among the confirmed SNe IIb.

After that, we collected images for all these distant SNe with the goal of investigating their unexpected location (see Fig. 12). The majority of them are in continuations of spiral arms, e.g. supernovae 1997dd or 2001cf. Exceptions are supernovae 2011ft and 2017gpn, which are well outside the borders of their host galaxies. We found Pan-STARRS 1 images (Chambers et al. 2016; Flewelling et al. 2016) for SN 2011ft in the r, i, z, and y passbands where one can notice a diffuse red object exactly at the SN 2011ft position, which can be associated with the host galaxy of SN 2011ft.

In addition, we consider the object with the highest relative separation in Fig. 11 (rel. sep. is 2.67; see Table A1), SN 2017ati, a candidate for type IIb SNe. It turns out that this SN exploded in a system of interacting galaxies. Due to this interaction, a region with a high star-formation rate could be formed, and this explains the detection of the core-collapse supernova far from the host galaxy disc. Therefore, SN 2017gpn is the only distant SNe that is not located in a region with a high star-formation rate.

According to the stellar evolution theory, the progenitor star of SN IIb should be a massive star with an initial mass of  $\sim 30 \text{ M}_{\odot}$ . The fact that SN 2017gpn exploded far from a region with a high star-formation rate challenges this popular scenario. We have considered three different hypotheses to explain its location.

First, the progenitor of SN 2017gpn could be a superspeed star. Brown et al. (2005) have discovered a hypervelocity star SDSS J090745.0+024507 with a mass of ~4 M<sub>☉</sub> ejected from the Milky Way centre and left with a velocity of 709 km s<sup>-1</sup>. If we presume that the SN 2017gpn progenitor mass is about 30 M<sub>☉</sub>, the average lifetime of such a star will be ~3 Myr, calculated by the formula  $t_{\rm life} \simeq \left(\frac{M_{\odot}}{M_{\rm star}}\right)^2$ . If it moves at a speed of 1000 km s<sup>-1</sup> (Hills 1988), it could move away from the centre of the host galaxy by ~29 kpc during its lifetime. However, such a high velocity implies that the kinetic energy is ~3 × 10<sup>50</sup> erg; therefore an effective mechanism of star acceleration is required.

The second hypothesis is that part of the spiral arm of the host galaxy NGC 1343 is faint and therefore cannot be easily observed. For example, a similar situation is observed for the object AM 1316–241 (Keel & White 2001; see Fig. 13). In this case we can see the faint spiral arm of the galaxy only because it is illuminated by the light of a background elliptical galaxy. It is important that this part of the spiral structure does not lie on the continuation of the bright spiral arm; therefore, a SN explosion there (in the absence of a 'lamp' behind) will appear to be outside the galaxy.

The third hypothesis is that the host galaxy of SN 2017gpn experienced an interaction with other galaxies in the past. Tidal force destroyed the satellite galaxy and provided enough gas, which could condense far from the NGC 1343 centre. Moreover, we can see the interaction between the galaxy ZOAG G134.74+13.65 and the SN 2017gpn host galaxy, which could also cause the formation of gas clouds with a high star-formation rate (see Fig. 12, panel 8).

#### 4.5 Connection with G299232

Initially SN 2017gpn was considered as a possible optical counterpart of the GW event G299232 since it was discovered 2 d later in its errorbox.<sup>4</sup> If we assume that gravitational energy is released by a collapse, GW events are expected from supernova explosions (Herant et al. 1994) and could be detected by the LIGO/Virgo experiment (The LIGO Scientific Collaboration et al. 2019).

<sup>4</sup>https://gcn.gsfc.nasa.gov/other/G299232.gcn3

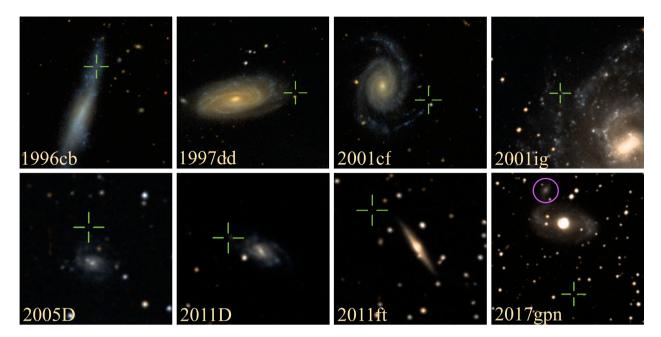
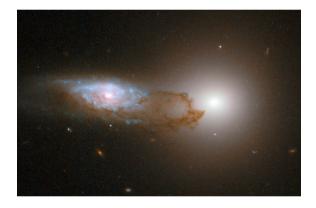


Figure 12. Optical images of supernovae distant from their host galaxy centres. SNe are marked by green crosses. All images were provided by SDSS (Blanton et al. 2017; Gunn et al. 1998) and DSS. The purple circle denotes the galaxy ZOAG G134.74+13.65.



**Figure 13.** An image of AM 1316–241 obtained by the *Hubble Space Telescope* (Keel & White 2001). The faint spiral arms are visible owing to the light from the background elliptical galaxy.

Nevertheless, the results of the hydrodynamic modelling show that the explosion happened on August 20 ( $\sim$ 3.5 d before the GW alert) following the best-fitting model, or on August 17 for the additional model, i.e.  $\sim$ 8 d before registration of G299232. G299232 is a lowsignificance event so it could be a false signal; even if it is not, it is still implausible that SN 2017gpn could be associated with this alert. Neither of our calculated models favour the electromagnetic counterpart of the gravitational event.

## **5 CONCLUSIONS**

In this paper we have presented spectroscopic and photometric observations of the type IIb supernova 2017gpn and the results of the numerical modelling of its *B*, *R* light curves with the STELLA code. The best-fitting hydrodynamic model has the following parameter values: pre-SN radius 50 R<sub> $\odot$ </sub>, pre-SN mass 3.5 M<sub> $\odot$ </sub>, mass of synthesized nickel totally mixed in the envelope 0.11 M<sub> $\odot$ </sub>, mass of the compact remnant 1.41 M<sub> $\odot$ </sub> (i.e. neutron star as a remnant), and energy of the explosion 1.2 × 10<sup>51</sup> erg. We also determined the

ranges for these parameters by considering the dependence of the modelled light curves on each parameter while the others remain fixed. The obtained ranges are 3–4  $M_{\odot}$  for the pre-SN mass, 20–70  $R_{\odot}$  for the pre-SN radius, 0.09–0.13  $M_{\odot}$  for the mass of <sup>56</sup>Ni, and, finally, (1.05–1.60) × 10<sup>51</sup> erg for  $E_{exp}$ .

The study of type IIb supernovae is an important part of the exploration of the chemical composition of the Universe. The nucleosynthesis yields of CCSNe including SNe IIb are characterized by strong contributions by the so-called alpha elements O, Ne, Mg, Si, S, Ar, Ca, and Ti (Thielemann et al. 2018) and the heavy elements, namely Ni, Co, and Fe.

According to the Open Supernova Catalog (Guillochon et al. 2017) only about a couple of dozen SNe IIb have detailed photometry that allows the performance of reliable hydrodynamic modelling. Some of these SNe are considered in this paper and compared with SN 2017gpn taking into account a physically motivated classification of stripped-envelope SNe proposed by Prentice & Mazzali (2017). In this classification SN 2017gpn belongs to the IIb(I) group, which is characterized by strong hydrogen line profiles before maximum light, which weaken greatly over time, and a H $\alpha$  P Cygni profile dominated by the absorption component. Analysis of the hydrodynamic modelling results of different SNe IIb shows that the mass of synthesized <sup>56</sup>Ni is in the range 0.05–0.15 M<sub> $\odot$ </sub>.

The modelling results for SN 2017gpn are consistent with those for SNe IIb considered, especially if we compare them with the modelling results for SN 2008ax, which is of group IIb(I) according to Prentice & Mazzali (2017). These results, together with the observational data presented here, contribute to the study of the type IIb SN phenomenon, increasing the sample of well-studied SNe IIb.

Finally, we considered three different hypotheses that could explain SN 2017gpn's distant location relative to its host galaxy:

(i) the progenitor of SN 2017gpn is a hypervelocity star ejected by NGC 1343 with an average speed more than 1000 km s<sup>-1</sup>;

(ii) the progenitor exploded in a faint spiral arm of the host galaxy;

(iii) the progenitor is formed in a region of interaction between the host galaxy and another galaxy in the past.

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## DATA AVAILABILITY

The data underlying this article are available in the article.

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#### **APPENDIX A: TABLE**

Table A1. A complete list of confirmed type IIb supernovae and candidates for SNe IIb.

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2.46 0.17	1 27
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2.780.263.111.353.771.392.460.17	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.111.353.771.392.460.17	
4       SN1997dd       16 05 46.33       +21 29 14.2       16 05 51.98       +21 29 05.9       0.0147       114.33       79.30       2         5       SN1998fa       06 42 51.51       +41 25 18.9       06 42 51.76       +41 25 19.4       0.0130       101.89       20.34         6       SN2000H       06 51 07.67       +12 55 18.5       06 51 06.28       +12 55 19.4       0.0130       101.89       20.34         7       SN2001g       13 13 23.89       +36 38 17.7       13 13 27.54       +43 63 53 7.1       0.0029       586.34       166.50         9       SN2001g       22 57 30.69       -41 02 25.9       22 57 18.36       -41 04 14.5       0.0031       300.71       176.76       1         10       SN2002g       19 49 47.25       +50 41 53.6       19 49 48.75       +50 41 46.0       0.0260       53.48       16.15         13       SN2003bg       04 10 59.43       -31 24 50.4       04 11 00.65       -31 24 7.8       0.0046       101.89       27.47         14       SN2003bg       11 17 48.30       +19 09 08.5       11 17 48.37       +19 09 05.4       0.0288       16.53       3.25         15       SN2003bg       10 01 9.47       -24 48 13.8       10 00 19.30	3.771.392.460.17	
5         SN1998fa         06 42 51.51         +41 25 18.9         06 42 51.76         +41 25 14.9         0.0250         57.3         4.89           6         SN2000H         06 51 07.67         +12 55 18.5         06 51 06.28         +41 03 15.0         0.0130         101.89         20.34           7         SN2001cf         12 02 31.64         +41 02 58.9         12 02 36.56         +41 03 15.0         0.0200         68.89         57.94         2           8         SN2001g         12 52 37 30.69         -41 02 25.9         22 57 18.36         -41 04 14.5         0.0021         300.71         176.76         1           10         SN2001Q         11 25 19.77         +63 43 15.6         11 25 19.05         +65 43 45.4         0.0124         140.65         30.18           11         SN2002u         09 34 37.60         +05 50 15.7         09 34 38.62         +05 50 29.2         0.0180         65.79         20.34           12         SN2002c         11 17 48.30         -31 24 50.4         04 11 00.65         -31 24 27.8         0.0046         101.89         27.47           14         SN2003cv         11 17 48.30         +19 09 08.5         111 7 48.37         +19 09 05.4         0.0288         16.53         3.25	2.46 0.17	23.77
6       SN200H       06 51 07.67       +12 55 18.5       06 51 06.28       +12 55 19.4       0.0130       101.89       20.34         7       SN2001cf       12 02 31.64       +41 02 28.9       12 02 36.56       +41 03 15.0       0.0200       68.89       57.94       2         8       SN2001gd       13 13 23.89       +36 38 17.7       13 13 27.54       +36 35 37.1       0.0029       586.34       166.50         9       SN2001g       11 25 19.77       +61 43 3 15.6       11 25 19.05       +63 43 45.4       0.0124       140.65       30.18         11       SN2002cu       09 34 37.60       +05 50 15.7       09 34 38.62       +05 50 29.2       0.0180       65.79       20.34         12       SN2003cg       19 49 47.25       +50 41 53.6       19 49 48.75       +50 41 46.0       0.0260       53.48       16.15         13       SN2003cv       11 17 48.30       +19 09 08.5       11 17 48.37       +19 09 05.4       0.0288       16.53       3.25         15       SN2003gu       23 02 59.45       +34 43 19.6       23 02 59.10       +34 43 37.7       0.0190       60.00       18.61         17       SN2003ki       07 51 33.24       +63 55 51.6       07 51 34.20       +63 55 42.0 </td <td></td> <td></td>		
7       SN2001cf       12 02 31.64       +41 02 58.9       12 02 36.56       +41 03 15.0       0.0200       68.89       57.94       2         8       SN2001gd       13 13 23.89       +36 38 17.7       13 13 27.54       +36 35 37.1       0.0029       586.34       166.50         9       SN2001ig       22 57 30.69       -41 02 25.9       22 57 18.36       -41 04 14.5       0.0031       300.71       176.76       11         10       SN2002au       09 34 37.60       +05 50 15.7       09 34 38.62       +05 50 29.2       0.0180       65.79       20.34         11       SN2003bg       04 10 59.43       -31 24 50.4       04 11 00.65       -31 24 27.8       0.0046       101.89       27.47         14       SN2003cu       11 3 47 45.40       +38 18 21.1       13 47 44.99       +38 18 16.4       0.0045       52.26       6.74         16       SN2003gu       23 02 59.45       +34 43 19.6       23 02 59.10       +34 43 37.7       0.0190       60.00       18.61         17       SN2003ki       07 51 33.24       +63 55 51.6       07 51 34.20       +63 55 24.20       0.0250       46.57       11.50         18       SN2004bi       10 047 37.45       +26 18 12.0       10 47 39.37 <td></td> <td>5.40</td>		5.40
8         SN2001gd         13 13 23.89         +36 38 17.7         13 13 27.54         +36 35 37.1         0.0029         586.34         166.50           9         SN2001ig         22 57 30.69         -41 02 25.9         22 57 18.36         -41 04 14.5         0.0031         300.71         176.76         1           10         SN2001Q         11 25 19.77         +63 43 15.6         11 25 19.05         +63 43 45.4         0.0124         140.65         30.18           11         SN2002au         09 34 37.60         +05 50 15.7         09 34 38.62         +05 50 29.2         0.0180         65.79         20.34           12         SN2003bg         04 10 59.43         -31 24 50.4         04 11 00.65         -31 24 27.8         0.0046         101.89         27.47           14         SN2003cv         11 17 48.30         +19 09 08.5         11 17 48.37         +19 09 05.4         0.0288         16.53         3.25           15         SN2003cd         13 47 45.40         +38 18 21.1         13 47 44.99         +38 18 16.4         0.0045         52.26         6.74           16         SN2003gu         23 02 59.45         +34 31 9.6         23 02 59.10         +34 43 37.7         0.0190         60.00         18.61		23.48
9         SN2001ig         22 57 30.69         -41 02 25.9         22 57 18.36         -41 04 14.5         0.0031         300.71         176.76         1           10         SN2001Q         11 25 19.77         +63 43 15.6         11 25 19.05         +63 43 45.4         0.0124         140.65         30.18           11         SN2002au         09 34 37.60         +05 50 15.7         09 34 38.62         +05 50 29.2         0.0180         65.79         20.34           12         SN2003bg         04 10 59.43         -31 24 50.4         04 11 00.65         -31 24 72.8         0.0046         101.89         27.47           14         SN2003cv         11 17 48.30         +19 09 08.5         11 17 48.37         +19 09 05.4         0.0288         16.53         3.25           15         SN2003gu         23 02 59.45         +34 43 19.6         23 02 59.10         +34 43 37.7         0.0190         60.00         18.61           17         SN2003ki         07 51 33.24         +63 55 51.6         07 51 34.20         +63 55 42.0         0.0250         46.57         11.50           18         SN2004be         10 00 19.47         -24 48 13.8         10 00 19.30         -24 48 08.0         0.0076         56.00         6.24		9.99
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14       SN2003cv       11 17 48.30       +19 09 08.5       11 17 48.37       +19 09 05.4       0.0288       16.53       3.25         15       SN2003ed       13 47 45.40       +38 18 21.1       13 47 44.99       +38 18 16.4       0.0045       52.26       6.74         16       SN2003gu       23 02 59.45       +34 43 19.6       23 02 59.10       +34 43 37.7       0.0190       60.00       18.61         17       SN2003ki       07 51 33.24       +63 55 51.6       07 51 34.20       +63 55 42.0       0.0250       46.57       11.50         18       SN2004be       10 00 19.47       -24 48 13.8       10 00 19.30       -24 48 08.0       0.0076       56.00       6.24         19       SN2004bi       10 47 37.45       +26 18 12.0       10 47 39.37       +26 17 41.5       0.0220       84.75       39.96       1         20       SN2004c       11 27 29.76       +56 52 48.4       11 27 31.89       +56 52 36.2       0.0057       104.27       21.30         21       SN2004ex       00 38 10.19       +02 43 17.2       00 38 12.38       +02 43 42.6       0.0180       111.73       41.50       1         23       SN2004ff       04 58 46.19       -21 34 12.0       04 58 47.12		2.61
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21       SN2004c       11 27 29.76       +56 52 48.4       11 27 31.89       +56 52 36.2       0.0057       104.27       21.30         22       SN2004ex       00 38 10.19       +02 43 17.2       00 38 12.38       +02 43 42.6       0.0180       111.73       41.50       1         23       SN2004ff       04 58 46.19       -21 34 12.0       04 58 47.12       -21 34 09.9       0.0230       73.82       13.14         24       SN2004gj       11 30 59.63       +20 28 06.8       11 31 00.66       +20 28 08.6       0.0210       44.48       14.59         25       SN2005D       07 26 57.36       +20 22 53.4       07 26 57.12       +20 22 15.5       0.0280       45.51       38.05       22         26       SN2005Em       03 13 47.71       -00 14 37.0       03 13 47.69       -00 14 36.7       0.0252       95.09       0.42         27       SN2005H       02 09 38.52       -10 08 43.6       02 09 38.56       -10 08 46.1       0.0128       80.94       2.57         28       SN2005U       11 28 33.22       +58 33 42.5       11 28 31.33       +58 33 41.8       0.0010       143.93       14.80         29       SN2006ba       09 43 13.40       -09 36 53.0       09 43 11.98		17.77
21       SN2004c       11 27 29.76       +56 52 48.4       11 27 31.89       +56 52 36.2       0.0057       104.27       21.30         22       SN2004ex       00 38 10.19       +02 43 17.2       00 38 12.38       +02 43 42.6       0.0180       111.73       41.50       1         23       SN2004ff       04 58 46.19       -21 34 12.0       04 58 47.12       -21 34 09.9       0.0230       73.82       13.14         24       SN2004gj       11 30 59.63       +20 28 06.8       11 31 00.66       +20 28 08.6       0.0210       44.48       14.59         25       SN2005D       07 26 57.36       +20 22 53.4       07 26 57.12       +20 22 15.5       0.0280       45.51       38.05       22         26       SN2005em       03 13 47.71       -00 14 37.0       03 13 47.69       -00 14 36.7       0.0252       95.09       0.42         27       SN2005H       02 09 38.52       -10 08 43.6       02 09 38.56       -10 08 46.1       0.0128       80.94       2.57         28       SN2005U       11 28 33.22       +58 33 42.5       11 28 31.33       +58 33 41.8       0.0010       143.93       14.80         29       SN2006ba       09 43 13.40       -09 36 53.0       09 43 11.98	0.56 0.09	0.56
22       SN2004ex       00 38 10.19       +02 43 17.2       00 38 12.38       +02 43 42.6       0.0180       111.73       41.50       1         23       SN2004ff       04 58 46.19       -21 34 12.0       04 58 47.12       -21 34 09.9       0.0230       73.82       13.14         24       SN2004gj       11 30 59.63       +20 28 06.8       11 31 00.66       +20 28 08.6       0.0210       44.48       14.59         25       SN2005D       07 26 57.36       +20 22 53.4       07 26 57.12       +20 22 15.5       0.0280       45.51       38.05       2         26       SN2005em       03 13 47.71       -00 14 37.0       03 13 47.69       -00 14 36.7       0.0252       95.09       0.42         27       SN2005H       02 09 38.52       -10 08 43.6       02 09 38.56       -10 08 46.1       0.0128       80.94       2.57         28       SN2005U       11 28 33.22       +58 33 42.5       11 28 31.33       +58 33 41.8       0.0010       143.93       14.80         29       SN2006ba       09 43 13.40       -09 36 53.0       09 43 11.98       -09 36 44.5       0.0190       106.70       22.66         30       SN2006bf       12 58 50.68       +09 39 30.1       12 58 50.91		2.50
23       SN2004ff       04 58 46.19       -21 34 12.0       04 58 47.12       -21 34 09.9       0.0230       73.82       13.14         24       SN2004gj       11 30 59.63       +20 28 06.8       11 31 00.66       +20 28 08.6       0.0210       44.48       14.59         25       SN2005D       07 26 57.36       +20 22 53.4       07 26 57.12       +20 22 15.5       0.0280       45.51       38.05       2         26       SN2005em       03 13 47.71       -00 14 37.0       03 13 47.69       -00 14 36.7       0.0252       95.09       0.42         27       SN2005H       02 09 38.52       -10 08 43.6       02 09 38.56       -10 08 46.1       0.0128       80.94       2.57         28       SN2005U       11 28 33.22       +58 33 42.5       11 28 31.33       +58 33 41.8       0.0010       143.93       14.80         29       SN2006ba       09 43 13.40       -09 36 53.0       09 43 11.98       -09 36 44.5       0.0190       106.70       22.66         30       SN2006bf       12 58 50.68       +09 39 30.1       12 58 50.91       +09 39 14.7       0.0240       57.30       15.77         31       SN2006el       22 47 38.50       +39 52 27.6       22 47 37.39       +39 52 44.8 <td>5.17 0.74</td> <td>15.17</td>	5.17 0.74	15.17
25       SN2005D       07 26 57.36       +20 22 53.4       07 26 57.12       +20 22 15.5       0.0280       45.51       38.05       2         26       SN2005em       03 13 47.71       -00 14 37.0       03 13 47.69       -00 14 36.7       0.0252       95.09       0.42         27       SN2005H       02 09 38.52       -10 08 43.6       02 09 38.56       -10 08 46.1       0.0128       80.94       2.57         28       SN2005U       11 28 33.22       +58 33 42.5       11 28 31.33       +58 33 41.8       0.0010       143.93       14.80         29       SN2006ba       09 43 13.40       -09 36 53.0       09 43 11.98       -09 36 44.5       0.0190       106.70       22.66         30       SN2006bf       12 58 50.68       +09 39 30.1       12 58 50.91       +09 39 14.7       0.0240       57.30       15.77         31       SN2006el       22 47 38.50       +39 52 27.6       22 47 37.39       +39 52 44.8       0.0170       47.66       21.43	6.10 0.36	6.10
25         SN2005D         07 26 57.36         +20 22 53.4         07 26 57.12         +20 22 15.5         0.0280         45.51         38.05         2           26         SN2005em         03 13 47.71         -00 14 37.0         03 13 47.69         -00 14 36.7         0.0252         95.09         0.42           27         SN2005H         02 09 38.52         -10 08 43.6         02 09 38.56         -10 08 46.1         0.0128         80.94         2.57           28         SN2005U         11 28 33.22         +58 33 42.5         11 28 31.33         +58 33 41.8         0.0010         143.93         14.80           29         SN2006ba         09 43 13.40         -09 36 53.0         09 43 11.98         -09 36 44.5         0.0190         106.70         22.66           30         SN2006bf         12 58 50.68         +09 39 30.1         12 58 50.91         +09 39 14.7         0.0240         57.30         15.77           31         SN2006el         22 47 38.50         +39 52 27.6         22 47 37.39         +39 52 44.8         0.0170         47.66         21.43	6.20 0.66	6.20
26SN2005em03 13 47.71-00 14 37.003 13 47.69-00 14 36.70.025295.090.4227SN2005H02 09 38.52-10 08 43.602 09 38.56-10 08 46.10.012880.942.5728SN2005U11 28 33.22+58 33 42.511 28 31.33+58 33 41.80.0010143.9314.8029SN2006ba09 43 13.40-09 36 53.009 43 11.98-09 36 44.50.0190106.7022.6630SN2006bf12 58 50.68+09 39 30.112 58 50.91+09 39 14.70.024057.3015.7731SN2006el22 47 38.50+39 52 27.622 47 37.39+39 52 44.80.017047.6621.43	1.38 1.67	21.38
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29         SN2006ba         09 43 13.40         -09 36 53.0         09 43 11.98         -09 36 44.5         0.0190         106.70         22.66           30         SN2006bf         12 58 50.68         +09 39 30.1         12 58 50.91         +09 39 14.7         0.0240         57.30         15.77           31         SN2006el         22 47 38.50         +39 52 27.6         22 47 37.39         +39 52 44.8         0.0170         47.66         21.43	0.67 0.06	0.67
30         SN2006bf         12 58 50.68         +09 39 30.1         12 58 50.91         +09 39 14.7         0.0240         57.30         15.77           31         SN2006el         22 47 38.50         +39 52 27.6         22 47 37.39         +39 52 44.8         0.0170         47.66         21.43	0.31 0.21	0.31
31         SN2006el         22 47 38.50         +39 52 27.6         22 47 37.39         +39 52 44.8         0.0170         47.66         21.43	8.73 0.42	8.73
	7.63 0.55	7.63
	7.41 0.90	7.41
32 SN2006iv 11 48 12.35 +54 59 14.6 11 48 11.32 +54 59 30.2 0.0081 88.75 17.94	2.99 0.40	2.99
33         SN2006qp         14 42 30.65         +28 43 25.9         14 42 33.24         +28 43 35.2         0.0120         119.72         35.32	8.67 0.59	8.67
34         SN2006T         09 54 30.21         -25 42 29.3         09 54 28.64         -25 42 11.8         0.0081         212.89         27.50	4.58 0.26	4.58
35 SN2007ay 08 17 14.85 +01 12 06.9 08 17 15.73 +01 12 23.0 0.0150 45.51 20.82	6.37 0.91	6.37
36 SN2008aq 12 50 30.42 -10 52 01.4 12 50 29.39 -10 51 15.7 0.0080 198.68 48.15	7.92 0.48	7.92
37         SN2008ax         12 30 40.80         +41 38 14.5         12 30 36.41         +41 38 37.4         0.0019         405.65         54.28	2.14 0.27	2.14
		12.32
39         SN2008bo         18 19 54.34         +74 34 20.9         18 19 46.42         +74 34 06.2         0.0049         198.68         34.86	3.53 0.35	3.53
40 SN2008cx 00 56 45.90 -09 54 19.0 00 56 42.66 -09 54 50.1 0.0189 134.32 57.09 2		21.89
41 SN2008ie 02 43 20.80 +04 58 19.1 02 43 22.27 +04 58 06.2 0.0137 140.65 25.47	7.13 0.36	7.13
	7.50 0.63	7.50
		11.43
44 SN2009jv 09 40 57.83 +47 37 04.0 09 40 58.19 +47 37 13.3 0.0161 90.81 9.99	3.27 0.22	3.27
	2.11 0.08	2.11
		6.52
		3.63
		2.14
		0.54
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A Contract of the second se		1.43
	6.00 1.00	16.80
54 SN2011dh 13 30 05.11 +47 10 10.9 13 29 52.70 +47 11 43.0 0.0016 828.23 156.49		5.19

 Table A1 – continued

56         SN2011 fu         02 08 21.40 $+41$ 29 12.3         02           57         SN2011 hs         22 57 11.77 $-43$ 23 04.8         22           58         SN2012 ht         59 05 04 $+01$ 59 04 $+01$ 53 24.4         15           59         SN2013 ak         08 07 06.69 $-28$ 03 10.1         08           61         SN2013 bh         14 12 13.96 $+15$ 50 31.5         14           63         SN2015 bi         14 32 15.31 $+26$ 19 32.0         14           64         SN2016 gkg         01 34 14.46 $-29$ 26 25.0         01           65         SN2016 gkg         01 34 14.46 $-29$ 26 62.0         01           66         SN2017 gpn         03 37 44.97 $+72$ 31 59.0         03           67         ASASSN-14az         23 44 48.00 $-02$ 07 03.2         23           68         ASASSN-14az         23 80 7.29 $+01$ 23 29.2         02           71         PTF1 liqb         00 34 04.84 $-09$ 42 17.9         00           72         SN2002 $z^h$ 04 13 12.5 $+13$ 25 07.3         04           75         SN200 $z^h$ 13 13 54.691 $+22$ 05 46	$A_{Host} \begin{bmatrix} h & m & s \\ \cdot & \cdot \end{bmatrix}$	Dec. <sub>Host</sub> [° ′ ″.]	z	D <sub>25</sub> [arcsec]	$\Theta$ [arcsec]	D [kpc]	Rel. sep
57SN2011hs2257II-432304.82258SN2012P14495990.4+105324.41559SN2013ak080706.69-280310.110861SN2013df122229.33+311338.31262SN2016adj132521.21-430057.91363SN2016gkg013414.46-292625.00164SN2016gkg013414.46-29265.00165SN2016gkg013414.46-29265.00166SN2017gpn033744.97+723159.00367ASASSN-14az234448.00-020703.22368ASASSN-14dq215759.7+241668.11170PS15cjr023807.29+012329.20271PTF1 ingb003404.84-094217.90072SN2001ad*172404+589520.01773SN2002br*041312.52+132507374SN2005br*134546.91+22056675SN2005br*14207.46+351142.714 <td>7 52 39.46</td> <td>+29 03 32.4</td> <td>0.0173</td> <td>62.83</td> <td>59.91</td> <td>21.07</td> <td>1.91</td>	7 52 39.46	+29 03 32.4	0.0173	62.83	59.91	21.07	1.91
58         SN2012P         14 59 59.04 $+01$ 53 24.4         15           59         SN2013ak         08 07 06.69 $-28$ 03 10.1         08           60         SN2013bb         14 12 13.96 $+15$ 50 31.5         14           61         SN2014ds         08 11 16.45 $+25$ 10 47.4         08           63         SN2015bi         14 32 15.31 $+26$ 19 32.0         14           64         SN2016gkg         01 34 14.46 $-29$ 26 25.0         01           65         SN2016gkg         01 34 14.46 $-29$ 26 25.0         01           66         SN2017gpn         03 74.97 $+72$ 31 59.0         03           67         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           68         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           69         ASASSN-160         13 12.52 $+13$ 25 07.3         04           71         PTF11igb         00 34 04.84 $-09$ 42 17.9         00           72         SN2002jz <sup>6</sup> 04 13 12.52 $+13$ 25 07.3         04           75         SN2002jz <sup>6</sup> 04 13 12.52 $+13$ 25 07.3         04	2 08 21.49	+41 28 45.1	0.0190	90.81	27.22	10.49	0.60
59         SN2013ak         08 07 06.69 $-28 03 10.1$ 08           50         SN2013bb         14 12 13.96 $+15 50 31.5$ 14           51         SN2013df         12 26 29.33 $+31 13 38.3$ 12           52         SN2016bi         14 22 15.31 $+26 19 32.0$ 14           54         SN2016bi         13 22 15.31 $+26 19 32.0$ 14           55         SN2017gpn         03 37 44.97 $+72 31 59.0$ 03           56         SN2017gpn         03 37 44.97 $+72 31 59.0$ 03           57         ASASSN-14da         21 57 59.97 $+24 16 08.1$ 21           50         ASASSN-14da         21 57 59.97 $+24 16 08.1$ 21           70         PS15cjr         02 38 07.29 $+01 23 29.2$ 02           71         PS15cjr         02 38 07.29 $+01 23 29.2$ 02           72         SN2002hz <sup>h</sup> 22 27 49.54 $+38 35 09.5$ 22           74         SN2005h <sup>h</sup> 13 45 46.91 $+22 05 46.8$ 13           75         SN2005h <sup>h</sup> 13 42 07.46 $+35 11 42.7$ 14	2 57 13.57	-43 23 46.1	0.0057	337.40	45.72	5.37	0.27
50         SN2013bb         14 12 13.96 $+15$ 50 31.5         14           51         SN2013df         12 26 29.33 $+31$ 13 38.3         12           52         SN2014ds         08 11 16.45 $+25$ 10 47.4         08           53         SN2015bi         14 32 15.31 $+26$ 19 32.0         14           54         SN2016gkg         01 34 14.46 $-29$ 26 25.0         01           55         SN2017gpn         03 37 44.97 $+72$ 31 59.0         03           56         SN2017gpn         03 37 44.97 $+72$ 31 59.0         03           59         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           59         ASASSN-14dq         21 57 59.97 $+21$ 16 08.1         21           70         PS15cjr         02 38 07.29         +01 23 29.2         02           71         SN2002hz <sup>b</sup> 04 13 12.52 $+13$ 25 07.3         04           75         SN2005hz <sup>b</sup> 13 45 46.91 $+22$ 05 46.8         13           76         SN2008cw <sup>b</sup> 16 32 38.27 $+41$ 27 33.2         16           73         SN2008gv <sup>b</sup> 10 15 32.95 $+74$ 12 59.1         10     <	5 00 00.43	+01 53 28.6	0.0045	181.20	21.26	1.98	0.23
51         SN2013df         12 26 29.33 $+31$ 13 38.3         12           52         SN2014ds         08 11 16.45 $+25$ 10 47.4         08           53         SN2015bi         14 32 15.31 $+26$ 19 32.0         14           54         SN2016adj         13 25 24.12 $-43$ 00 57.9         13           55         SN2016gkg         01 34 14.46 $-29$ 26 25.0         01           56         SN2017gpn         03 37 44.97 $+72$ 31 59.0         03           57         ASASSN-14az         23 44 48.00 $-02$ 07 03.2         23           58         ASASSN-15bd         15 54 38.33 $+16$ 36 38.1         15           50         PS15cjr         02 38 07.29 $+01$ 23 29.2         02           71         PTF11igb         00 44.84 $-09$ 42 17.9         00           72         SN2002jz <sup>b</sup> 04 13 12.52 $+13$ 25 07.3         04           73         SN2002jz <sup>b</sup> 04 13 12.52 $+13$ 25 07.3         04           74         SN2002jz <sup>b</sup> 07 11 39.03 $-26$ 42 20.2         07           75         SN2005w <sup>b</sup> 10 15 32.95 $+74$ 12 59.1         10 <td>8 07 08.00</td> <td>-28 03 08.0</td> <td>0.0037</td> <td>140.65</td> <td>17.47</td> <td>1.34</td> <td>0.25</td>	8 07 08.00	-28 03 08.0	0.0037	140.65	17.47	1.34	0.25
52         SN2014ds         08 11 16.45 $+25$ 10 47.4         08           53         SN2015bi         14 32 15.31 $+26$ 19 32.0         14           54         SN2016adj         13 25 24.12 $-43$ 00 57.9         13           55         SN2017gpn         03 37 44.97 $+72$ 31 59.0         03           56         SN2017gpn         03 37 44.97 $+72$ 31 59.0         03           57         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           59         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           59         ASASSN-14dq         21 57 59.97 $+24$ 16 08.1         21           71         PS15cjr         02 38 07.29 $+01$ 23 29.2         02           71         SN2001ad <sup>b</sup> 72 44 02.40 $+58$ 55 50.0         17           73         SN2005b <sup>b</sup> 13 45 46.91 $+22$ 05 46.8         13           74         SN2005b <sup>b</sup> 13 42 52.7 $+41$ 27 33.2         16           75         SN2005b <sup>b</sup> 16 32 38.27 $+41$ 27 33.2         16           76         SN2008g <sup>b</sup> 10 32 35.57         -04 02 36.0         03	4 12 15.81	+15 50 30.9	0.0175	70.49	26.70	9.50	0.76
53SN2015bi14 32 15.31 $+26$ 19 32.01454SN2016adj13 25 24.12 $-43$ 00 57.91355SN2017gpn03 37 44.97 $+72$ 31 59.00356SN2017gpn03 37 44.97 $+72$ 31 59.00357ASASSN-14az23 44 48.00 $-02$ 07 03.22358ASASSN-14dq21 57 59.97 $+24$ 16 08.12159ASASSN-15bd15 54 38.33 $+16$ 36 38.11570PS15cjr02 38 07.29 $+01$ 23 29.20271PTF11iqb00 34 04.84 $-09$ 42 17.90072SN2001ad <sup>b</sup> 17 24 02.40 $+58$ 59 52.01773SN2002bz <sup>b</sup> 04 13 12.52 $+13$ 25 07.30475SN2005bz <sup>b</sup> 13 45 46.91 $+22$ 05 46.81376SN2005bz <sup>b</sup> 14 20 27.46 $+35$ 11 42.71478SN2008gx <sup>b</sup> 16 15 23.95 $+74$ 12 59.11080SN2009gj <sup>b</sup> 00 30 28.56 $-33$ 12 56.00081SN2009gj <sup>b</sup> 00 30 28.57 $-04$ 02 30.21483SN2011br <sup>b</sup> 22 47 07.49 $-64$ 49 43.42284SN2011br <sup>b</sup> 22 47 07.49 $-64$ 49 43.42285SN2011cb <sup>b</sup> 22 47 07.49 $-64$ 49 43.42286SN2011br <sup>b</sup> 23 11 48.44+31 01 0.0.42387SN2011br <sup>b</sup> 23 47 07.49 $-64$ 49 43.42286SN2011br <sup>b</sup> 22 47 07.49 $-64$ 49 43.422	2 26 27.09	+31 13 24.8	0.0024	116.99	31.75	1.58	0.54 0.33
54         SN2016adj         13 25 24.12 $-43 00 57.9$ 13           55         SN2016kg         01 34 14.46 $-29 26 25.0$ 01           56         SN2017gpn         03 37 44.97 $+72 31 59.0$ 03           57         ASASSN-14dq         21 57 59.97 $+24 16 08.1$ 21           59         ASASSN-14dq         21 57 59.97 $+24 16 08.1$ 21           50         PS15cjr         02 38 07.29 $+01 23 29.2$ 00           71         PTF1 ligb         00 44 4.84 $-09 42 17.9$ 00           72         SN2001zb <sup>2</sup> 22 7 49.54 $+38 35 09.5$ 22           74         SN2002jz <sup>b</sup> 01 41 31 2.52 $+13 25 07.3$ 04           75         SN2005lx <sup>b</sup> 13 4 5 46.91 $+22 05 46.8$ 13           76         SN2008sv <sup>b</sup> 16 23 38.27 $+41 27 33.2$ 16           78         SN2008gv <sup>b</sup> 10 15 32.95 $+74 12 59.1$ 10           80         SN2009gv <sup>b</sup> 14 01 53.61 $-01 20 30.2$ 14           79         SN2008gv <sup>b</sup> 13 02 53.57 $-04 04 23.4$ 2	8 11 15.92 4 32 15.19	+25 10 45.7 +26 19 36.2	0.0137 0.0160	44.48 42.48	7.39 4.50	2.07 1.47	0.33
55         SN2016gkg         01 34 14.46 $-292625.0$ 01           56         SN2017gpn         03 37 44.97 $+723159.0$ 03           57         ASASSN-14az         23 44 48.00 $-020703.2$ 23           58         ASASSN-14dg         215759.97 $+241608.1$ 21           59         ASASSN-15bd         15 54 38.33 $+163638.1$ 15           70         PS15cjr         02 38 07.29 $+012329.2$ 00           72         SN2002hz <sup>b</sup> 22 27 49.54 $+383509.5$ 22           73         SN2002hz <sup>b</sup> 22 27 49.54 $+383509.5$ 22           74         SN2005by <sup>b</sup> 13 45 46.91 $+220546.8$ 13           75         SN2008cw <sup>b</sup> 10 15 32.95 $+74123.2$ 10           76         SN2008gx <sup>b</sup> 10 15 32.95 $+741259.1$ 10           78         SN2008gx <sup>b</sup> 10 30 25.56 $-331256.0$ 00           81         SN2008gx <sup>b</sup> 10 15 32.95 $+741259.1$ 10           78         SN2008gx <sup>b</sup> 10 30 2 53.57 $-040236.0$ 12	4 32 13.19 3 25 27.60	$-43\ 01\ 08.8$	0.0018	42.48	4.50 39.69	1.47	0.21
56SN2017pm033744.97+723159.00357ASASSN-14az2323448.00 $-02$ 0703.22358ASASSN-14dq215759.97+241608.12159ASASSN-15bd155438.33+161636.811570PS15cjr0202807.29+012329.20271PTF11qb003404.84 $-09$ 4217.90072SN2001ab172402.40+585952.01773SN2002jzb041312.52+132507.30476SN2005byb134546.91+220546.81377SN2006sgb142027.46+351142.71478SN2009ggb062148.6-5942.600681SN2009ggb062148.6-5942.600682SN2009ggb062148.6-5942.600683SN2010jrb051935.80-323928.20584SN2011brb132235.57-040236.02285SN2011brb233057.02+152924.32386SN2011brb233057.2+152924.323 <td>1 34 18.24</td> <td><math>-29\ 25\ 06.6</math></td> <td>0.0018</td> <td>322.22</td> <td>92.66</td> <td>9.37</td> <td>0.58</td>	1 34 18.24	$-29\ 25\ 06.6$	0.0018	322.22	92.66	9.37	0.58
57       ASASSN-14az       23 44 48.00 $-02$ 07 03.2       23         58       ASASSN-14dq       21 57 59.97 $+24$ 16 08.1       21         59       ASASSN-15bd       15 54 38.33 $+16$ 36 38.1       15         50       PS15cjr       02 38 07.29 $+01$ 23 29.2       02         71       PTF11iqb       00 34 04.84 $-09$ 42 17.9       00         72       SN2001zb <sup>b</sup> 22 27 49.54 $+38$ 55 09.5       22         74       SN2002jz <sup>b</sup> 04 13 12.52 $+13$ 25 07.3       04         75       SN2005bv <sup>b</sup> 13 45 46.91 $+22$ 05 46.8       13         76       SN2008cs <sup>b</sup> 10 15 32.95 $+74$ 12 7 33.2       16         79       SN2008cs <sup>b</sup> 10 15 32.95 $+74$ 12 59.1       10         80       SN2009g <sup>b</sup> 00 30 28.56 $-33$ 12 56.0       00         81       SN2009g <sup>b</sup> 05 19 35.80 $-32$ 39 28.2       05         82       SN2010g <sup>b</sup> 05 19 35.80 $-32$ 39 28.2       05         83       SN2010g <sup>b</sup> 02 47 7.49 $-64$ 49 43.4       22         84       SN2011b <sup>b</sup> 23 11 48.84 $+31$ 01 00.4	3 37 49.72	+72 34 16.6	0.0074	143.93	139.25	21.20	1.93
58         ASASSN-14dq         21         57         9.97 $+24$ 16         36         1         15           59         ASASSN-15bd         15         54         38.33 $+16$ 36         38.1         15           70         PS15cjr         02         38         07.29 $+01$ 23         29.2         00           71         PTF1         1igb         00         40.484 $-09$ 42         17.9         00           72         SN2002hz <sup>b</sup> 22         27         49.54 $+38$ 35         09.5         22           74         SN2005by <sup>b</sup> 13         45         6.91 $+22$ 05         46.8         13           75         SN2006ss <sup>b</sup> 14         20         7.46 $+35$ 11         42.7         14           78         SN2008gx <sup>b</sup> 10         15         32.95 $+74$ 12         59.1         10           80         SN2008gx <sup>b</sup> 10         15         32.95 $+74$ 12         59.1         10         30         23         23.2         10         33	3 44 48.27	$-02\ 06\ 53.4$	0.0067	38.74	10.6	1.46	0.55
59       ASASSN-15bd       15 54 38.33       +16 36 38.1       15         70       PS15cjr       02 38 07.29       +01 23 29.2       02         71       PTF11iqb       00 34 04.84       -09 42 17.9       00         72       SN2001ad <sup>b</sup> 22 27 49.54       +38 35 09.5       22         74       SN2002jz <sup>b</sup> 04 13 12.52       +13 25 07.3       04         75       SN2005by <sup>b</sup> 13 45 46.91       +22 05 46.8       13         76       SN2005by <sup>b</sup> 16 32 38.27       +41 27 33.2       16         77       SN2008cw <sup>b</sup> 16 32 38.27       +41 27 9.1       10         80       SN2009gj <sup>b</sup> 00 30 28.56       -33 12 56.0       00         81       SN2009gj <sup>b</sup> 05 19 35.80       -32 39 28.2       05         82       SN2010jr <sup>b</sup> 05 19 35.80       -32 39 28.2       05         83       SN2011br <sup>b</sup> 23 057.02       +15 29 24.3       23         84       SN2011br <sup>b</sup> 23 057.02       +15 29 24.3       23         85       SN2011cb <sup>b</sup> 23 11 48.84       +31 01 00.4       23         86       SN2011cb <sup>b</sup> 23 11 48.84       +31 01 00.4       23      <	1 57 59.82	+24 15 59.7	0.0104	79.10	8.65	1.84	0.22
71PTF11iqb00 34 04.84 $-09$ 42 17.90072SN2001ad <sup>b</sup> 17 24 02.40 $+58$ 59 52.01773SN2002bz <sup>b</sup> 22 27 49.54 $+38$ 35 09.52274SN2002jz <sup>b</sup> 04 13 12.52 $+13$ 25 07.30475SN2005by <sup>b</sup> 13 45 46.91 $+22$ 05 46.81376SN2008ss <sup>b</sup> 16 32 38.27 $+41$ 27 33.21677SN2008cs <sup>b</sup> 16 32 38.27 $+41$ 27 33.21678SN2008gb <sup>b</sup> 10 15 32.95 $+74$ 12 59.11080SN2009gi <sup>b</sup> 00 30 28.56 $-33$ 12 56.00081SN2009grb <sup>b</sup> 06 21 44.86 $-59$ 44 26.00682SN2009grb <sup>b</sup> 06 21 32 53.57 $-04$ 02 36.083SN2010jrb <sup>b</sup> 05 19 35.80 $-32$ 39 28.20584SN2011brb <sup>b</sup> 13 02 53.57 $-04$ 02 36.085SN2011cb <sup>b</sup> 22 47 07.49 $-64$ 49 43.42286SN2011ei <sup>b</sup> 23 30 57.02 $+15$ 29 24.32387SN2012cd <sup>b</sup> 13 22 35.25 $+54$ 48 47.01390SN2012dy <sup>b</sup> 21 18 50.70 $-57$ 38 42.52191SN2012gb <sup>b</sup> 09 20 53.46 $-64$ 54 19.70992SN2012brb <sup>b</sup> 09 02 05.46 $-44$ 34 40.00885SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.71490SN2012brb <sup>b</sup> 09 20 25.46 $-64$ 54 19.70992SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.714 <td< td=""><td>5 54 38.39</td><td>+16 36 37.6</td><td>0.0080</td><td>22.81</td><td>1.00</td><td>0.16</td><td>0.09</td></td<>	5 54 38.39	+16 36 37.6	0.0080	22.81	1.00	0.16	0.09
72SN2001adb17 24 02.40+58 59 52.01773SN2002hzb22 27 49.54+38 35 09.52274SN2002jzb04 13 12.52+13 25 07.30475SN2005byb13 45 46.91+22 05 46.81376SN2005kb14 20 27.46+35 11 42.71478SN2008cwb16 32 38.27+41 27 33.21679SN2008gxb10 15 32.95+74 12 59.11080SN2009gjb00 30 28.56-33 12 56.00081SN2009gbb06 21 44.86-59 44 26.00682SN2010gbb05 19 35.80-32 39 28.20583SN2010jbb05 19 35.80-32 39 28.20584SN2011bbb13 02 53.57-04 02 36.02485SN2011cbb22 47 07.49-64 49 43.42286SN2011cbb23 30 57.02+15 29 24.32387SN2012cdb13 22 35.25+54 48 47.01389SN2012cdb13 22 35.25+54 48 47.01390SN2012cdb90 20 5.46-64 54 19.70992SN2012cbb09 20 25.46-64 54 19.70993SN2013cbb09 49 14.71-47 54 45.60994SN2013cbb09 23 29.55-63 40 28.30995SN2013cbb09 23 29.55-63 40 28.30996SN2013cbb09 23 29.55-63 40 28.30997SN2013cbb09 23 29.55-63 40 28.309 </td <td>2 38 07.57</td> <td>+01 23 18.1</td> <td>0.0229</td> <td>72.14</td> <td>11.87</td> <td>5.49</td> <td>0.33</td>	2 38 07.57	+01 23 18.1	0.0229	72.14	11.87	5.49	0.33
73SN2002hzb22 27 49.54+38 35 09.52274SN2002jzb04 13 12.52+13 25 07.30475SN2005byb13 45 46.91+22 05 46.81376SN2005bb07 11 39.03-26 42 20.20777SN2006scb14 20 27.46+35 11 42.71478SN2008gxb10 15 32.95+74 12 59.11080SN2009gib00 30 28.56-33 12 56.00081SN2009gib06 21 44.86-59 44 26.00682SN2009grb16 01 53.61-01 20 30.21483SN2010jrb05 19 35.80-32 39 28.20584SN2011cbb22 47 07.49-64 49 43.42285SN2011cbb20 34 22.62-31 58 23.62086SN2011cfb23 11 48.84+31 01 00.42387SN2012cdb13 22 35.25+54 48 47.01389SN2012cdb13 22 35.25+54 48 47.01390SN2012grb09 20 54.6-64 54 19.70992SN2013cub90 20 54.6-64 54 19.70993SN2013cub14 33 58.97+40 14 20.71494SN2013cub14 33 58.97+40 14 20.71495SN2013cub19 59 07.95-55 54 6.61996SN2013cub19 59 07.95-55 54 6.61997SN2013cub10 25 47.80-11 25 17.61098SN2014cdp09 23 29.55-63 40 28.309	0 34 02.79	-09 42 19.0	0.0125	157.82	30.33	7.75	0.38
74       SN2002jz <sup>b</sup> 04 13 12.52       +13 25 07.3       04         75       SN2005ly <sup>b</sup> 13 45 46.91       +22 05 46.8       13         76       SN2005ly <sup>b</sup> 14 20 27.46       +35 11 42.7       14         77       SN2008sy <sup>b</sup> 16 32 38.27       +41 27 33.2       16         79       SN2008gx <sup>b</sup> 10 15 32.95       +74 12 59.1       10         80       SN2009gj <sup>b</sup> 00 30 28.56       -33 12 56.0       00         81       SN2009mb <sup>b</sup> 06 21 44.86       -59 44 26.0       06         82       SN2009Z <sup>b</sup> 14 01 53.61       -01 20 30.2       14         83       SN2010Jr <sup>b</sup> 05 19 35.80       -32 39 28.2       05         84       SN2011le <sup>b</sup> 22 47 07.49       -64 49 43.4       22         85       SN2011le <sup>b</sup> 23 10 57.02       +15 29 24.3       23         86       SN2011le <sup>b</sup> 23 11 48.84       +31 01 00.4       23         80       SN2012d <sup>b</sup> 21 18 50.70       -57 38 42.5       21         91       SN2012d <sup>b</sup> 92 13 2.0       09         92       SN2012ly <sup>b</sup> 91 14 33 58.97       +40 14 20.7       14         93<	7 24 08.11	+585942.4	0.0110	61.40	45.15	10.17	1.47
75       SN2005 $y^b$ 13 45 46.91       +22 05 46.8       13         76       SN2005 $h^b$ 07 11 39.03       -26 42 20.2       07         77       SN2006s $s^b$ 14 20 27.46       +35 11 42.7       14         78       SN2008 $x^b$ 10 15 32.95       +74 12 59.1       10         79       SN2009 $g^b$ 00 30 28.56       -33 12 56.0       00         81       SN2009 $g^b$ 06 21 44.86       -59 44 26.0       06         82       SN201 $g^b$ 05 19 35.80       -32 39 28.2       05         83       SN201 $lg^b$ 02 47 07.49       -64 49 43.4       22         84       SN2011 $le^b$ 22 47 07.49       -64 49 43.4       22         85       SN2011 $le^b$ 23 47 07.49       -64 49 43.4       22         86       SN2011 $le^b$ 23 11 48.84       +31 01 00.4       23         87       SN2012 $le^b$ 13 22 35.25       +54 48 47.0       13         80       SN2012 $le^b$ 91 24 37.95       +49 21 32.0       09         91       SN2012 $le^b$ 90 20 54.6       -64 54 19.7       09         92       SN2013 $cu^b$ 14 33 58.97       +40 14 20.7       14 <td>2 27 48.30</td> <td>+38 35 11.7</td> <td>0.0180</td> <td>99.58</td> <td>14.70</td> <td>5.38</td> <td>0.30</td>	2 27 48.30	+38 35 11.7	0.0180	99.58	14.70	5.38	0.30
76       SN20051 <sup>b</sup> 07 11 39.03 $-264220.2$ 07         77       SN2006ss <sup>b</sup> 14 20 27.46 $+351142.7$ 14         78       SN2008gx <sup>b</sup> 10 15 32.95 $+741259.1$ 10         79       SN2009gi <sup>b</sup> 00 30 28.56 $-331256.0$ 00         80       SN2009gi <sup>b</sup> 06 21 44.86 $-594426.0$ 06         82       SN2009Z <sup>b</sup> 14 01 53.61 $-012030.2$ 14         83       SN2010jr <sup>b</sup> 05 19 35.80 $-323928.2$ 05         84       SN2011bv <sup>b</sup> 13 02 53.57 $-040236.0$ 22         85       SN2011cb <sup>b</sup> 22 47 07.49 $-644943.4$ 22         86       SN2011e <sup>b</sup> 23 30 57.02 $+152924.3$ 23         87       SN2011e <sup>b</sup> 20 34 22.62 $-318823.6$ 20         88       SN2011g <sup>b</sup> 09 42 37.95 $+492132.0$ 09         90       SN2012g <sup>b</sup> 09 20 25.46 $-645419.7$ 09         91       SN2012g <sup>b</sup> 09 49 14.71 $-475445.6$ 09         92       SN2013g <sup>b</sup> 14 33 58.97 $+401420.7$ 14	4 13 12.40	+13 25 19.1	0.0052	60.00	11.93	1.28	0.40
77       SN2006ss <sup>b</sup> 14 20 27.46       +35 11 42.7       14         78       SN2008gx <sup>b</sup> 16 32 38.27       +41 27 33.2       16         79       SN2008gx <sup>b</sup> 10 15 32.95       +74 12 59.1       10         80       SN2009gi <sup>b</sup> 00 30 28.56       -33 12 56.0       00         81       SN2009gi <sup>b</sup> 06 21 44.86       -59 44 26.0       06         82       SN2009Z <sup>b</sup> 14 01 53.61       -01 20 30.2       14         83       SN201jr <sup>b</sup> 05 19 35.80       -32 39 28.2       05         84       SN2011cb <sup>b</sup> 22 47 07.49       -64 49 43.4       22         85       SN2011ei <sup>b</sup> 23 30 57.02       +15 29 24.3       23         86       SN2011ei <sup>b</sup> 23 31 14 8.84       +31 01 00.4       23         87       SN2012cd <sup>b</sup> 13 22 35.25       +54 48 47.0       13         90       SN2012cd <sup>b</sup> 21 18 50.70       -57 38 42.5       21         91       SN2012g <sup>b</sup> 09 12 05.46       -64 54 19.7       09         92       SN2012al <sup>b</sup> 09 02 05.46       -64 54 19.7       14         93       SN2012al <sup>b</sup> 14 33 58.97       +40 14 20.7       14	3 45 45.62	+22 05 18.4	0.0270	75.54	33.59	18.22	0.89
78       SN2008cw <sup>b</sup> 16 32 38.27       +41 27 33.2       16         79       SN2008gx <sup>b</sup> 10 15 32.95       +74 12 59.1       10         80       SN2009gi <sup>b</sup> 00 30 28.56       -33 12 56.0       00         81       SN2009Z <sup>b</sup> 14 01 53.61       -01 20 30.2       14         82       SN2009Z <sup>b</sup> 14 01 53.61       -01 20 30.2       14         83       SN201jr <sup>b</sup> 05 19 35.80       -32 39 28.2       05         84       SN2011cb <sup>b</sup> 22 47 07.49       -64 49 43.4       22         85       SN2011ei <sup>b</sup> 22 47 07.49       -64 49 43.4       22         86       SN2011ei <sup>b</sup> 23 30 57.02       +15 29 24.3       23         87       SN2011ei <sup>b</sup> 23 34 22.62       -31 58 23.6       20         88       SN2011ei <sup>b</sup> 23 31 14 8.84       +31 01 00.4       23         89       SN2012cd <sup>b</sup> 13 12 32.5       +54 48 47.0       13         90       SN2012cd <sup>b</sup> 13 12 35.25       +44 847.0       13         91       SN2012cd <sup>b</sup> 09 02 05.46       -64 54 19.7       09         92       SN2013cu <sup>b</sup> 14 33 58.97       +40 14 20.7       14 <td>7 11 40.45</td> <td>-26 42 17.9</td> <td>0.0086</td> <td>125.36</td> <td>19.17</td> <td>3.39</td> <td>0.31</td>	7 11 40.45	-26 42 17.9	0.0086	125.36	19.17	3.39	0.31
39SN2008gx <sup>b</sup> 10 15 32.95 $+74$ 12 59.110 $30$ SN2009gj <sup>b</sup> 00 30 28.56 $-33$ 12 56.000 $31$ SN2009Z <sup>b</sup> 14 01 53.61 $-01$ 20 30.214 $33$ SN2010jr <sup>b</sup> 05 19 35.80 $-32$ 39 28.205 $34$ SN2011bv <sup>b</sup> 13 02 53.57 $-04$ 02 36.0 $55$ SN2011cb <sup>b</sup> 22 47 07.49 $-64$ 49 43.422 $46$ SN2011ei <sup>b</sup> 20 34 22.62 $-31$ 58 23.620 $37$ SN2011ei <sup>b</sup> 20 34 22.62 $-31$ 58 23.620 $38$ SN2012cd <sup>b</sup> 13 22 35.25 $+54$ 48 47.013 $49$ SN2012cd <sup>b</sup> 21 18 50.70 $-57$ 38 42.521 $91$ SN2012g <sup>b</sup> 09 20 5.46 $-64$ 54 19.709 $92$ SN2012b <sup>b</sup> 09 49 14.71 $-47$ 54 45.609 $94$ SN2012b <sup>b</sup> 09 49 14.71 $-47$ 54 45.619 $94$ SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.714 $96$ SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.714 $96$ SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.714 $96$ SN2013cu <sup>b</sup> 12 58 30.35 $+40$ 25 44.522 $97$ SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.714 $96$ SN2013cu <sup>b</sup> 12 53 55 $-63$ 40 28.309 $99$ SN2014cd <sup>b</sup> 09 23 29.55 $-63$ 40 28.309 $99$ SN2014cd <sup>b</sup> 10 25 47.80 $-11$ 25 17.610 $03$ SN2016bu <sup>b</sup> 10 25 47.80	4 20 26.50	+35 11 19.1	0.0120	88.75	26.37	6.48	0.59
30 $SN200^{\circ}gj^{b}$ 003028.56 $-33$ 1256.00031 $SN2009mg^{b}$ 062144.86 $-59$ 4426.00632 $SN2009Z^{b}$ 140153.61 $-01$ 2030.21433 $SN2010jr^{b}$ 051935.80 $-32$ 3928.20534 $SN2011bv^{b}$ 130253.57 $-04$ 0236.035 $SN2011cb^{b}$ 224707.49 $-64$ 4943.42236 $SN2011ef^{b}$ 233057.02 $+15$ 2924.32337 $SN2011ef^{b}$ 233148.84 $+31$ 010.42339 $SN2012dv^{b}$ 211850.70 $-57$ 3842.52190 $SN2012dy^{b}$ 211850.70 $-67$ 3842.52191 $SN2012fy^{b}$ 092437.95 $+49$ 2132.00992 $SN2012hb^{b}$ 09202.46 $-44$ 5419.70993 $SN2012hb^{b}$ 09225830.35 $+40$ 2544.52294 $SN2013cu^{b}$ 143358.97 $+40$ 1420.71495 $SN2014dr^{b}$ 092329.55 $-63$ 4028.30996 $SN2014dr^{b}$ 092329.55 $-63$ 4028.30	6 32 38.00	+41 27 33.0	0.0320	25.59	3.04	1.94	0.24
81SN2009mgb06 21 44.86 $-59$ 44 26.00682SN2009Zb14 01 53.61 $-01$ 20 30.21483SN2010jrb05 19 35.80 $-32$ 39 28.20584SN2011bvb13 02 53.57 $-04$ 02 36.02285SN2011cb22 47 07.49 $-64$ 49 43.42286SN2011eib20 34 22.62 $-31$ 58 23.62087SN2011eib20 34 22.62 $-31$ 58 23.62088SN2012dyb21 18 50.70 $-57$ 38 42.52190SN2012dyb21 18 50.70 $-57$ 38 42.52191SN2012fgb09 24 37.95 $+49$ 21 32.00992SN2012hb09 02 05.46 $-64$ 54 19.70993SN2012hb09 49 14.71 $-47$ 54 45.60994SN2013clb09 49 14.71 $-47$ 54 45.60995SN2013cub14 33 58.97 $+40$ 14 20.71496SN2013cub14 33 58.97 $+40$ 14 20.71497SN2013fqb19 59 07.95 $-55$ 55 46.61998SN2014cqb09 23 29.55 $-63$ 40 28.30999SN2014ab08 11 16.45 $+25$ 10 47.48100SN2015mb10 25 47.80 $-11$ 25 17.610103SN2016bhsb07 38 05.53 $-55$ 11 47.007104SN2016bhsb10 25 47.80 $-11$ 25 17.610105SN2016bhsb07 38 95.51 $-29$ 01 26.411116SN2016bhsb	0 15 32.22	+74 13 13.1	0.0215	67.32	14.31	6.22	0.43
32SN2009Z <sup>b</sup> 14 01 53.61 $-01 20 30.2$ 14 $33$ SN2010jr <sup>b</sup> 05 19 35.80 $-32 39 28.2$ 05 $34$ SN2011bv <sup>b</sup> 13 02 53.57 $-04 02 36.0$ $35$ SN2011cb <sup>b</sup> 22 47 07.49 $-64 49 43.4$ 22 $36$ SN2011ei <sup>b</sup> 20 34 22.62 $-31 58 23.6$ 20 $38$ SN2011g <sup>b</sup> 23 11 48.84 $+31 01 00.4$ 23 $39$ SN2012cd <sup>b</sup> 13 22 35.25 $+54 48 47.0$ 13 $300$ SN2012dy <sup>b</sup> 21 18 50.70 $-57 38 42.5$ 21 $901$ SN2012fg <sup>b</sup> 09 24 37.95 $+49 21 32.0$ 09 $922$ SN2012hb <sup>b</sup> 09 02 05.46 $-64 54 19.7$ 09 $923$ SN2012hb <sup>b</sup> 09 49 14.71 $-47 54 45.6$ 09 $944$ SN2013h <sup>b</sup> 08 46 15.06 $+41 34 40.0$ 08 $925$ SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 14 $926$ SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 14 $926$ SN2013cu <sup>b</sup> 19 59 07.95 $-55 55 46.6$ 19 $928$ SN2014cd <sup>b</sup> 09 23 29.55 $-63 40 28.3$ 09 $929$ SN2014ds <sup>b</sup> 08 11 16.45 $+25 10 47.4$ 8 $920$ SN2016av <sup>b</sup> 10 25 47.80 $-11 25 17.6$ 10 $930$ SN2016av <sup>b</sup> 10 25 47.80 $-11 25 17.6$ 10 $941$ SN2016bhr <sup>b</sup> 14 25 20.58 $+32 28 55.9$ 14 $940$ SN2016bhr <sup>b</sup> 14 25 20.58 $+32 28 55.9$ 14 $940$ SN2016bhr <sup>b</sup> <t< td=""><td>0 30 21.89</td><td>-33 14 43.3</td><td>0.0053</td><td>499.06</td><td>136.08</td><td>14.88</td><td>0.55</td></t<>	0 30 21.89	-33 14 43.3	0.0053	499.06	136.08	14.88	0.55
33SN2010jr <sup>b</sup> 05 19 35.80 $-32$ 39 28.20534SN2011bv <sup>b</sup> 13 02 53.57 $-04$ 02 36.035SN2011cb <sup>b</sup> 22 47 07.49 $-64$ 49 43.42236SN2011ef <sup>b</sup> 23 30 57.02 $+15$ 29 24.32337SN2011ef <sup>b</sup> 20 34 22.62 $-31$ 58 23.62038SN2012cd <sup>b</sup> 13 22 35.25 $+54$ 48 47.01339SN2012dy <sup>b</sup> 21 18 50.70 $-57$ 38 42.52191SN2012fg <sup>b</sup> 09 24 37.95 $+49$ 21 32.00992SN2012bb <sup>b</sup> 09 20 05.46 $-64$ 54 19.70992SN2012bb <sup>b</sup> 09 20 05.46 $-64$ 54 19.70992SN2012b <sup>b</sup> 09 49 14.71 $-47$ 54 45.60994SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.71495SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.71496SN2013ep <sup>b</sup> 22 58 30.35 $+40$ 25 44.52297SN2013fq <sup>b</sup> 19 59 07.95 $-55$ 55 46.61998SN2014cq <sup>b</sup> 09 23 29.55 $-63$ 40 28.30999SN2016ab <sup>b</sup> 07 38 05.53 $-55$ 11 47.00704SN2015y <sup>b</sup> 09 02 37.87 $+25$ 56 04.20902SN2016ab <sup>b</sup> 11 08 55.51 $-29$ 01 26.41105SN2016bh <sup>b</sup> 14 25 20.58 $+32$ 28 55.91405SN2016bh <sup>b</sup> 14 25 20.58 $+32$ 28 55.91406SN2016bh <sup>b</sup> 17 80 55.1 $-29$ 01 26.411<	6 21 38.91	-59 44 24.0	0.0076	143.93	45.02	7.04	0.63
44SN2011bv <sup>b</sup> 13 02 53.57 $-04 02 36.0$ 55SN2011cb <sup>b</sup> 22 47 07.49 $-64 49 43.4$ 2256SN2011et <sup>b</sup> 23 30 57.02 $+15 29 24.3$ 2357SN2011et <sup>b</sup> 20 34 22.62 $-31 58 23.6$ 2058SN2011cd <sup>b</sup> 13 12 35.25 $+54 48 47.0$ 1359SN2012dv <sup>b</sup> 21 18 50.70 $-57 38 42.5$ 2191SN2012fg <sup>b</sup> 09 24 37.95 $+49 21 32.0$ 0992SN2012bb <sup>b</sup> 09 02 05.46 $-64 54 19.7$ 0993SN2012bb <sup>b</sup> 09 49 14.71 $-47 54 45.6$ 0994SN2013bl <sup>b</sup> 08 46 15.06 $+41 34 40.0$ 0895SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 1496SN2013ep <sup>b</sup> 22 58 30.35 $+40 25 44.5$ 2297SN2013fq <sup>b</sup> 19 59 07.95 $-55 55 46.6$ 1998SN2014ds <sup>b</sup> 08 11 16.45 $+25 10 47.4$ 800SN2015au <sup>b</sup> 22 30 59.42 $-13 59 56.1$ 2201SN2016avh <sup>b</sup> 10 25 47.80 $-11 25 17.6$ 1003SN2016bhs <sup>b</sup> 07 38 05.53 $-55 11 47.0$ 0704SN2016bhs <sup>b</sup> 11 85 5.51 $-29 01 26.4$ 1105SN2016bhs <sup>b</sup> 11 85 5.51 $-29 01 26.4$ 1106SN2016bhs <sup>b</sup> 15 85 9.71 $-32 22 18.5$ 0107SN2016bhs <sup>b</sup> 07 30 39 34.38 $+20 42 30.4$ 0310SN2016bhs <sup>b</sup> 01 58 59.71 $-32 22 18.5$ 01<	4 01 53.80	-01 20 35.6	0.0101		0.00	0.00	0.01
35SN2011cb <sup>b</sup> $22 47 07.49$ $-64 49 43.4$ $22$ 36SN2011ef <sup>b</sup> 23 30 57.02 $+15 29 24.3$ 2337SN2011ei <sup>b</sup> 20 34 22.62 $-31 58 23.6$ 2038SN2012cd <sup>b</sup> 13 22 35.25 $+54 48 47.0$ 1339SN2012dy <sup>b</sup> 21 18 50.70 $-57 38 42.5$ 2191SN2012fg <sup>b</sup> 09 24 37.95 $+49 21 32.0$ 0992SN2012hb <sup>b</sup> 09 02 05.46 $-64 54 19.7$ 0993SN2012hb <sup>b</sup> 09 04 91 4.71 $-47 54 45.6$ 0994SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 1495SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 1496SN2013ep <sup>b</sup> 22 58 30.35 $+40 25 44.5$ 2297SN2013fq <sup>b</sup> 19 59 07.95 $-55 55 46.6$ 1998SN2014cq <sup>b</sup> 09 23 29.55 $-63 40 28.3$ 0999SN2014ds <sup>b</sup> 08 11 16.45 $+25 10 47.4$ 800SN2015u <sup>b</sup> 09 02 37.87 $+25 56 04.2$ 0902SN2016avh <sup>b</sup> 10 25 47.80 $-11 25 17.6$ 1003SN2016bhr <sup>b</sup> 14 25 20.58 $+32 28 55.9$ 1405SN2016bhr <sup>b</sup> 14 25 20.58 $+32 28 55.9$ 1406SN2016bhr <sup>b</sup> 17 20 24.3 $+32 51 01.2$ 0708SN2016bhr <sup>b</sup> 01 58 59.71 $-32 22 18.5$ 0109SN2016bhr <sup>b</sup> 01 20 834.23 $+29 14 11.1$ 0211SN2016bhr <sup>b</sup> 01 26 87.5 $-77 38 15.0$ </td <td>5 19 35.81</td> <td>-32 39 27.9</td> <td>0.0124</td> <td>82.82</td> <td>0.33</td> <td>0.08</td> <td>0.01</td>	5 19 35.81	-32 39 27.9	0.0124	82.82	0.33	0.08	0.01
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77SN2011ei <sup>b</sup> 20 34 22.62 $-31 58 23.6$ 2088SN2011hg <sup>b</sup> 23 11 48.84 $+31 01 00.4$ 2399SN2012cd <sup>b</sup> 13 22 35.25 $+54 48 47.0$ 1390SN2012hg <sup>b</sup> 21 18 50.70 $-57 38 42.5$ 2191SN2012hg <sup>b</sup> 09 24 37.95 $+49 21 32.0$ 0992SN2012hb <sup>b</sup> 09 02 05.46 $-64 54 19.7$ 0993SN2012hb <sup>b</sup> 09 49 14.71 $-47 54 45.6$ 0994SN2013bl <sup>b</sup> 08 46 15.06 $+41 34 40.0$ 0895SN2013cu <sup>b</sup> 14 33 58.97 $+40 14 20.7$ 1496SN2013gp <sup>b</sup> 22 58 30.35 $+40 25 44.5$ 2297SN2013fq <sup>b</sup> 19 59 07.95 $-55 55 46.6$ 1998SN2014cq <sup>b</sup> 09 23 29.55 $-63 40 28.3$ 0999SN2014as <sup>b</sup> 08 11 16.45 $+25 10 47.4$ 800SN2015au <sup>b</sup> 22 30 59.42 $-13 59 56.1$ 2201SN2015u <sup>b</sup> 09 02 37.87 $+25 56 04.2$ 0902SN2016avh <sup>b</sup> 10 25 47.80 $-11 25 17.6$ 1003SN2016bhr <sup>b</sup> 14 25 20.58 $+32 28 55.9$ 1405SN2016bhr <sup>b</sup> 14 25 20.58 $-42 30.4$ 0310SN2016bhr <sup>b</sup> 14 55 5.71 $-29 01 26.4$ 1104SN2016bhr <sup>b</sup> 14 55 5.71 $-32 22 18.5$ 0105SN2016bhr <sup>b</sup> 14 55 5.71 $-32 22 18.5$ 0109SN2016bhr <sup>b</sup> 07 45 19.72 $-71 24 17.9$ 07 </td <td>2 47 06.26</td> <td>-64 49 55.4</td> <td>0.0079</td> <td>261.91</td> <td>14.34</td> <td>2.33</td> <td>0.11</td>	2 47 06.26	-64 49 55.4	0.0079	261.91	14.34	2.33	0.11
88SN2011hgb231148.84+310100.42389SN2012cdb132235.25+544847.01390SN2012dyb211850.70-573842.52191SN2012fgb092437.95+492132.00992SN2012hbb09205.46-645419.70993SN2012hbb094435584425.42294SN2013cub143358.97+401420.71495SN2013cub143358.97+401420.71496SN2013cub1225830.35+402544.52297SN2013fqb19590.79-555546.61998SN2014cqb092329.55-634028.30999SN2014abb088116.45+251047.4800SN2015Yb090237.87+255604.20902SN2016avhb102547.80-112517.61003SN2016bhb142520.58+322855.91405SN2016bhb141545.76-473815.01406SN2016bhb141545.76-473815	3 30 56.80	$+15\ 29\ 26.0$	0.0134	64.29	3.61 34.29	0.99	0.11 0.24
39SN2012cd <sup>b</sup> 13 22 35.25 $+54 \ 48 \ 47.0$ 1330SN2012dy <sup>b</sup> 21 18 50.70 $-57 \ 38 \ 42.5$ 2191SN2012fg <sup>b</sup> 09 24 37.95 $+49 \ 21 \ 32.0$ 0992SN2012hb <sup>b</sup> 09 02 05.46 $-64 \ 54 \ 19.7$ 0993SN2012hb <sup>b</sup> 09 49 14.71 $-47 \ 54 \ 45.6$ 0994SN2013hl <sup>b</sup> 08 \ 46 \ 15.06 $+41 \ 34 \ 40.0$ 0895SN2013cu <sup>b</sup> 14 \ 33 \ 58.97 $+40 \ 14 \ 20.7$ 1496SN2013cu <sup>b</sup> 19 \ 59 \ 07.95 $-55 \ 55 \ 46.6$ 1997SN2013fq <sup>b</sup> 19 \ 59 \ 07.95 $-55 \ 55 \ 46.6$ 1998SN2014cq <sup>b</sup> 09 \ 23 \ 29.55 $-63 \ 40 \ 28.3$ 0999SN2014ds <sup>b</sup> 08 \ 11 \ 16.45 $+25 \ 10 \ 47.4$ 800SN2015au <sup>b</sup> 22 \ 30 \ 59.42 $-13 \ 59 \ 56.1$ 2201SN2016av <sup>b</sup> 10 \ 25 \ 47.80 $-11 \ 25 \ 17.6$ 1003SN2016av <sup>b</sup> 10 \ 25 \ 47.80 $-11 \ 25 \ 17.6$ 1003SN2016bv <sup>b</sup> 10 \ 25 \ 47.80 $-11 \ 25 \ 17.6$ 1004SN2016bv <sup>b</sup> 14 \ 25 \ 20.58 $+32 \ 28 \ 55.9$ 1405SN2016bv <sup>b</sup> 11 \ 08 \ 55.51 $-29 \ 01 \ 26.4$ 1106SN2016bv <sup>b</sup> 11 \ 85 \ 59.71 $-32 \ 22 \ 18.5$ 0107SN2016bv <sup>b</sup> 01 \ 58 \ 59.71 $-32 \ 21 \ 85.0$ 1407SN2016bv <sup>b</sup> 01 \ 58 \ 59.71 $-32 \ 21 \ 85.0$ 1407SN2016bv <sup>b</sup>	0 34 21.00 3 11 50.29	$-31\ 58\ 51.0$ +31\ 01\ 16.2	0.0093 0.0236	280.64 92.93	24.44	6.55 11.64	0.24
00SN2012dyb $21 18 50.70$ $-57 38 42.5$ $21$ $01$ SN2012fgb $09 24 37.95$ $+49 21 32.0$ $09$ $02$ SN2012hbb $09 02 05.46$ $-64 54 19.7$ $09$ $03$ SN2012hbb $09 49 14.71$ $-47 54 45.6$ $09$ $03$ SN2013hb $08 46 15.06$ $+41 34 40.0$ $08$ $05$ SN2013cb $14 33 58.97$ $+40 14 20.7$ $14$ $06$ SN2013cpb $12 25 8 30.35$ $+40 25 44.5$ $22$ $07$ SN2013fqb $19 59 07.95$ $-55 55 46.6$ $199$ $08$ SN2014cqb $09 23 29.55$ $-63 40 28.3$ $09$ $09$ SN2014dsb $08 11 16.45$ $+25 10 47.4$ $8$ $100$ SN2015aub $22 30 59.42$ $-13 59 56.1$ $22$ $101$ SN2016avb $10 25 47.80$ $-11 25 17.6$ $100$ $102$ SN2016bavb $07 38 05.53$ $-55 11 47.0$ $07$ $104$ SN2016bhrb $14 25 20.58$ $+32 28 55.9$ $14$ $105$ SN2016bhrb $14 15 45.76$ $-47 38 15.0$ $14$ $106$ SN2016bhrb $11 08 55.51$ $-29 01 26.4$ $11$ $108$ SN2016bhrb $07 33 9 34.38$ $+20 42 30.4$ $03$ $110$ SN2016bhrb $07 45 19.72$ $-71 24 17.9$ $07$ $113$ SN2016bhrb $07 45 19.72$ $-71 24 17.9$ $07$ $114$ SN2016bhrb $07 45 19.72$ $-71 24 17.9$ $07$ $113$ SN2016bhrb $07 45 19.72$ $-71 24 17.9$	3 22 32.43	+51 01 10.2 +54 49 05.0	0.0230	92.93 51.07	30.30	7.32	1.19
D1SN2012fgb09 24 37.95+49 21 32.009D2SN2012hbb09 02 05.46-64 54 19.709D3SN2012hsb09 49 14.71-47 54 45.609D4SN2013blb08 46 15.06+41 34 40.008D5SN2013cub14 33 58.97+40 14 20.714D6SN2013epb22 58 30.35+40 25 44.522D7SN2013fqb19 59 07.95-55 55 46.619D8SN2014cqb09 23 29.55-63 40 28.309D9SN2014dsb08 11 16.45+25 10 47.48100SN2015aub22 30 59.42-13 59 56.122101SN2015Yb09 02 37.87+25 56 04.209102SN2016avhb10 25 47.80-11 25 17.610103SN2016bhrb14 25 20.58+32 28 55.914105SN2016bhrb14 15 45.76-47 38 15.014106SN2016bhrb14 15 45.76-47 38 15.014107SN2016bhrb10 28 34.23+29 11 41.102108SN2016bhrb17 85 59.71-32 22 18.501109SN2016bkrb07 20 24.3+32 51 01.207108SN2016bhrb17 85 59.71-32 22 18.501109SN2016bkrb07 45 19.72-71 24 17.907111SN2016bkrb07 45 19.72-71 24 17.907113SN2016bkrb07 16 37.75+67 53 32.307114SN2016brb10 34 19.27	1 18 50.99	$-57\ 38\ 25.2$	0.0118	128.28	30.30 17.46	3.69	0.27
$22$ SN2012hb <sup>b</sup> $09\ 02\ 05.46$ $-64\ 54\ 19.7$ $09\ 02$ $23$ SN2012hs <sup>b</sup> $09\ 49\ 14.71$ $-47\ 54\ 45.6$ $09\ 04$ $24$ SN2013bl <sup>b</sup> $08\ 46\ 15.06$ $+41\ 34\ 40.0$ $08\ 25$ $25$ SN2013cu <sup>b</sup> $14\ 33\ 58.97$ $+40\ 14\ 20.7$ $14\ 20.7$ $26$ SN2013ep <sup>b</sup> $22\ 58\ 30.35$ $+40\ 25\ 44.5$ $22\ 27\ 7$ $27$ SN2013fq <sup>b</sup> $19\ 59\ 07.95$ $-55\ 55\ 46.6$ $19\ 28\ 8$ $28$ SN2014cq <sup>b</sup> $09\ 23\ 29.55$ $-63\ 40\ 28.3$ $09\ 29\ 80\ 80\ 201\ 46.6$ $29$ SN2014ds <sup>b</sup> $08\ 11\ 16.45\ +25\ 10\ 47.4$ $8\ 20\ 80\ 201\ 59\ 56\ 12\ 22\ 10\ 47.4$ $200$ SN2015au <sup>b</sup> $22\ 30\ 59.42\ -13\ 59\ 56\ 12\ 22\ 100\ 10\ 50\ 80\ 201\ 50\ 50\ -11\ 25\ 17.6\ 100\ 20\ 80\ 201\ 50\ 50\ -11\ 25\ 17.6\ 100\ 20\ 50\ 20\ 20\ 50\ 50\ -11\ 25\ 17.6\ 100\ 20\ 20\ 20\ 20\ 20\ 20\ 20\ 20\ 20\ $	9 24 37.73	$+49\ 21\ 25.5$	0.0163	128.28	6.85	2.27	0.12
$33$ SN2012hs^b09 49 14.71 $-47$ 54 45.609 $94$ SN2013bl^b08 46 15.06 $+41$ 34 40.008 $95$ SN2013cu^b14 33 58.97 $+40$ 14 20.714 $96$ SN2013ep^b22 58 30.35 $+40$ 25 44.522 $97$ SN2013fq^b19 59 07.95 $-55$ 55 46.619 $98$ SN2014cq^b09 23 29.55 $-63$ 40 28.309 $99$ SN2014ds^b08 11 16.45 $+25$ 10 47.48 $100$ SN2015u^b22 30 59.42 $-13$ 59 56.122 $101$ SN2015Y^b09 02 37.87 $+25$ 56 64.209 $102$ SN2016avh^b10 25 47.80 $-11$ 25 17.610 $103$ SN2016bas^b07 38 05.53 $-55$ 11 47.007 $104$ SN2016bhr^b14 25 20.58 $+32$ 28 55.914 $105$ SN2016bhr^b14 15 45.76 $-47$ 38 15.014 $106$ SN2016bhr^b14 15 45.76 $-47$ 38 15.014 $107$ SN2016bhr^b07 20 24.3 $+32$ 51 01.207 $108$ SN2016bhr^b01 58 59.71 $-32$ 22 18.501 $109$ SN2016bhr^b02 08 34.23 $+29$ 14 11.102 $111$ SN2016bhr^b07 45 19.72 $-71$ 24 17.907 $113$ SN2016hr^b07 16 37.75 $+67$ 53 32.307 $114$ SN2016hr^b07 45 19.27 $-71$ 24 17.907 $113$ SN2016hr^b10 34 19.27 $+03$ 24 25.510 $115$ SN2017aca^b19	9 02 05.52	-64 54 16.2	0.0056	80.94	3.52	0.41	0.09
04SN2013blb08 46 15.06+41 34 40.00805SN2013cub14 33 58.97+40 14 20.71406SN2013epb22 58 30.35+40 25 44.52207SN2013fqb19 59 07.95 $-55 55 46.6$ 1908SN2014cqb09 23 29.55 $-63 40 28.3$ 0909SN2014dsb08 11 16.45+25 10 47.4800SN2015aub22 30 59.42 $-13 59 56.1$ 2201SN2015Yb09 02 37.87+25 56 04.20902SN2016avhb10 25 47.80 $-11 25 17.6$ 1003SN2016basb07 38 05.53 $-55 11 47.0$ 0704SN2016blrb14 15 45.76 $-47 38 15.0$ 1405SN2016blrb14 15 45.76 $-47 38 15.0$ 1406SN2016blrb10 158 59.71 $-32 22 18.5$ 0107SN2016blrb10 158 59.71 $-32 22 18.5$ 0108SN2016blrb07 39 34.38 $+20 42 30.4$ 0310SN2016blrb07 45 19.72 $-71 24 17.9$ 0713SN2016blrb10 34 19.27 $+03 24 25.5$ 1014SN2016iycb02 09 44.20 $+41 7 41.1$ 0215SN2017acab19 24 02.19 $+42 17 21.1$ 1917SN2017adb16 45 38.967 $+01 37 19.7$ 1618SN2017eiyb23 49 28.27 $-30 25 04.7$ 2319SN2017fekb20 21 47.44 $-10 43 53.3$ 20	9 49 16.53	-47 55 12.9	0.0064	111.73	32.86	4.33	0.59
95SN2013cu <sup>b</sup> 14 33 58.97 $+40$ 14 20.71496SN2013ep <sup>b</sup> 22 58 30.35 $+40$ 25 44.52297SN2013fq <sup>b</sup> 19 59 07.95 $-55$ 55 46.61998SN2014cq <sup>b</sup> 09 23 29.55 $-63$ 40 28.30999SN2014ds <sup>b</sup> 08 11 16.45 $+25$ 10 47.48100SN2015u <sup>b</sup> 22 30 59.42 $-13$ 59 56.122101SN2015Y <sup>b</sup> 09 02 37.87 $+25$ 56 04.209102SN2016avh <sup>b</sup> 10 25 47.80 $-11$ 25 17.610103SN2016bas <sup>b</sup> 07 38 05.53 $-55$ 11 47.007104SN2016bhr <sup>b</sup> 14 25 20.58 $+32$ 28 55.914105SN2016bhr <sup>b</sup> 14 15 45.76 $-47$ 38 15.014106SN2016bhr <sup>b</sup> 11 85 55.1 $-29$ 01 26.411107SN2016bhr <sup>b</sup> 10 20 24.3 $+32$ 51 01.207108SN2016bhr <sup>b</sup> 01 58 59.71 $-32$ 22 18.501109SN2016bhr <sup>b</sup> 02 08 34.23 $+29$ 14 11.102111SN2016iyc <sup>b</sup> 02 08 34.23 $+29$ 14 11.102111SN2016iyc <sup>b</sup> 07 45 19.72 $-71$ 24 17.907113SN2016iyc <sup>b</sup> 10 34 19.27 $+03$ 24 25.510115SN2017ati <sup>b</sup> 09 49 56.70 $+67$ 10 59.609116SN2017cao <sup>b</sup> 19 24 02.19 $+42$ 17 21.119117SN2017ati <sup>b</sup> 09 49 56.70 $+67$ 10 37 19.716118SN2017eiy <sup>b</sup> 23 49 28.27 <td>8 46 14.07</td> <td>+41 34 47.5</td> <td>0.0304</td> <td>62.83</td> <td>13.40</td> <td>8.15</td> <td>0.43</td>	8 46 14.07	+41 34 47.5	0.0304	62.83	13.40	8.15	0.43
266SN2013ep <sup>b</sup> $225830.35$ $+402544.5$ $222$ $277$ SN2013fq <sup>b</sup> 195907.95 $-555546.6$ 19 $28$ SN2014cq <sup>b</sup> 092329.55 $-634028.3$ 09 $299$ SN2014ds <sup>b</sup> 081116.45 $+251047.4$ 8 $100$ SN2015u <sup>b</sup> 223059.42 $-135956.1$ 22 $101$ SN2015Y <sup>b</sup> 090237.87 $+255604.2$ 09 $102$ SN2016avh <sup>b</sup> 102547.80 $-112517.6$ 10 $103$ SN2016bhr <sup>b</sup> 142520.58 $+322855.9$ 14 $105$ SN2016bhr <sup>b</sup> 14855.51 $-290126.4$ 11 $106$ SN2016bhr <sup>b</sup> 072024.3 $+325101.2$ 07 $108$ SN2016bhr <sup>b</sup> 015859.71 $-322218.5$ 01 $109$ SN2016bhr <sup>b</sup> 02834.23 $+291411.1$ 02 $100$ SN2016bhr <sup>b</sup> 074519.72 $-712417.9$ 07 $110$ SN2016bhr <sup>b</sup> 074519.72 $-712417.9$ 07 $111$ SN2016iyc <sup>b</sup> 020834.23 $+291411.1$ 02 $111$ SN2016iyc <sup>b</sup> 192402.19 $+421721.1$ 19 $113$ SN2016U <sup>b</sup> 1064319.27 $-70224.7$ $-712417.9$ 07 $113$ SN2016U <sup>b</sup> 1064319.27 $-712417.9$ 07 $114$ SN2017ai <sup>b</sup> 094956.70 $+671059.6$ 09 $115$ SN2017ai <sup>b</sup> 094956.70 $+6713719.7$ 16 $116$ SN2017eg <sup>b</sup> 234928.27 $-302504.7$ 23 $119$ SN2017fek <sup>b</sup> 202147.44 $-104353.3$	4 33 59.00	$+40\ 14\ 40.0$	0.0252	67.32	19.30	9.80	0.57
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 58 29.31	+40 25 46.3					
$98$ SN2014 $cq^b$ $09$ 23 29.55 $-63$ 40 28.3 $09$ $99$ SN2014 $ds^b$ $08$ 11 16.45 $+25$ 10 47.4 $8$ $100$ SN2015 $u^b$ $22$ 30 59.42 $-13$ 59 56.1 $22$ $101$ SN2015 $u^b$ $09$ 02 37.87 $+25$ 56 04.2 $09$ $102$ SN2016 $avh^b$ $10$ 25 47.80 $-11$ 25 17.6 $100$ $103$ SN2016 $bas^b$ $07$ 38 05.53 $-55$ 11 47.0 $07$ $104$ SN2016 $bhr^b$ $14$ 25 20.58 $+32$ 28 55.9 $14$ $105$ SN2016 $bhr^b$ $14$ 25 20.58 $+32$ 28 55.9 $14$ $106$ SN2016 $bhr^b$ $14$ 15 45.76 $-47$ 38 15.0 $14$ $107$ SN2016 $bhr^b$ $07$ 20 24.3 $+32$ 51 01.2 $07$ $108$ SN2016 $bhr^b$ $01$ 58 59.71 $-32$ 22 18.5 $01$ $109$ SN2016 $bkr^b$ $01$ 58 59.71 $-32$ 22 18.5 $01$ $109$ SN2016 $bkr^b$ $02$ 08 34.23 $+29$ 14 11.1 $02$ $111$ SN2016 $bkr^b$ $02$ 08 34.23 $+29$ 14 11.1 $02$ $111$ SN2016 $bkr^b$ $07$ 45 19.72 $-71$ 24 17.9 $07$ $113$ SN2016 $bkr^b$ $07$ 45 37.5 $+67$ 53 32.3 $07$ $114$ SN2016 $btr^b$ $10$ 34 19.27 $+03$ 24 25.5 $100$ $115$ SN2017 $ati^b$ $09$ 49 56.70 $+67$ 10 59.6 $09$ $116$ SN2017 $ati^b$ $09$ 49 56.70 $+67$ 10 59.6 $09$ $117$ SN2017 $ati^b$ $09$ 49 2.19 $+42$ 17 2.1.1 $19$ <t< td=""><td>9 59 06.40</td><td>-55 55 41.6</td><td></td><td></td><td></td><td></td><td></td></t<>	9 59 06.40	-55 55 41.6					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 23 26.79	-63 40 45.3	0.0110	109.18	25.02	5.64	0.46
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3 11 15.92	+25 10 45.7	0.0137	44.48	7.39	2.07	0.33
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 30 59.91	$-14\ 00\ 12.8$	0.0160	122.50	18.16	5.92	0.30
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 02 38.64	+25 56 04.5	0.0080	84.75	10.39	1.71	0.25
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 25 48.97	-11 25 28.5	0.0380	43.47	20.36	15.35	0.94
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7 38 05.53	-55 11 26.7	0.0090	128.28	20.30	3.75	0.32
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 25 20.59	+32 28 56.5	0.0139	32.97	0.61	0.17	0.04
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 08 55.52	-29 01 25.5					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4 15 45.64	-47 38 27.7	0.0160	79.10	12.76	4.16	0.32
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7 20 24.60	$+32\ 50\ 58.8$					
	1 59 00.57	$-32\ 22\ 25.2$					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3 39 34.78	+20 42 31.9	0.0212	36.15	5.81	2.49	0.32
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2 08 34.37	+29 14 02.6	0.0219	36.15	8.70	3.85	0.48
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2 09 15.30	+21 31 06.8	0.0127	49.91	18.71	4.86	0.75
14 $SN2016U^b$ 10 34 19.27 $+03 24 25.5$ 1015 $SN2017ati^b$ 09 49 56.70 $+67 10 59.6$ 0916 $SN2017cao^b$ 19 24 02.19 $+42 17 21.1$ 1917 $SN2017dgd^b$ 16 45 38.967 $+01 37 19.7$ 1618 $SN2017eiy^b$ 23 49 28.27 $-30 25 04.7$ 2319 $SN2017fek^b$ 20 21 47.44 $-10 43 53.3$ 20	7 45 15.96	-71 24 37.6	0.0180	90.81	26.67	9.75	0.59
	7 16 36.07	+67 53 42.2	0.0360	27.43	13.71	9.81	1.00
$      \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	0 34 19.10	$+03\ 24\ 22.9$	0.0740	21.78	3.64	5.12	0.33
117SN2017dgd^b16 45 38.967 $+01 37 19.7$ 16118SN2017eiy^b23 49 28.27 $-30 25 04.7$ 23119SN2017fek^b20 21 47.44 $-10 43 53.3$ 20	9 49 50.40	+67 11 11.0	0.0131	28.72	38.38	10.27	2.67
18SN2017eiyb23 49 28.27 $-30 25 04.7$ 2319SN2017fekb20 21 47.44 $-10 43 53.3$ 20	9 24 02.15	+42 17 27.6	0.0200	23.34	6.52	2.64	0.56
119 SN2017fek <sup>b</sup> 20 21 47.44 $-10$ 43 53.3 20	6 45 39.02	$+01\ 37\ 13.1$	0.0470	15 51	11 10	10.21	0.40
	3 49 28.64	$-30\ 25\ 14.8$	0.0470	45.51	11.18	10.31	0.49
$120$ SN2017 of $b^{p}$ 20.03.27.40 $\pm 0.6.50.27.2$ 20	0 21 47.70	-104346.0	0.0330	49.91	8.24	5.43	0.33
	0 03 27.78 0 12 51.80	$+06\ 59\ 22.8$ $-32\ 44\ 02.0$	0.0245 0.0600	51.07 18.54	7.17 9.07	3.54 10.52	0.28 0.98

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 Table A1 – continued

	No.	SN name	$RA_{SN} [^{h m s}]$	Dec. <sub>SN</sub> [° ′ ″.]	$RA_{Host} \; [{}^{h \; m \; s} \; ]$	Dec. <sub>Host</sub> [° ′ ″.]	z	D <sub>25</sub> [arcsec]	$\Theta$ [arcsec]	D [kpc]	Rel. sep.
124         SN2017m/sh <sup>4</sup> 0 71 04.07         +-06 27 14.4         07 10 40.48         +-06 27 13.0         0.0120         39.64         22.7.3         7.30         1.50           125         SN2017y4 <sup>6</sup> 11 40 25.00         +-01 59 33.1         11 46 24.70         +01 59 39.6         0.0285         19.42         7.00         4.52         0.81           128         SN2017gh <sup>6</sup> 10 23 45.51         +53 10 62.05         10 23 46.90         +53 10 62.80         0.0317         4.53         1.45.9         9.2.4         0.64           130         SN2017mv <sup>6</sup> 09 57 20.97         -41 35 21.0         09 57 20.90         -41 35 28.0         0.0117         57.30         7.44         1.60         0.52           131         SN2018mv <sup>6</sup> 10 10 25.16         +0.21 34.88         10 10 27.86         +0.21 34.16         0.0217         58.63         7.17         4.85         0.42           133         SN2018m <sup>6</sup> 14 06 34.70         -0.57 70.29         14 06 34.89         -0.57 10.7         0.0095         137.45         8.30         1.62         0.12           134         SN2018m <sup>6</sup> 25 05 20.5         -54 44.66         0.0243         7.36         2.82         1.40         1.63         0.224 <td>122</td> <td></td> <td>09 13 44.37</td> <td>+76 28 42.4</td> <td>09 13 43.04</td> <td></td> <td></td> <td></td> <td></td> <td>1.23</td> <td>0.16</td>	122		09 13 44.37	+76 28 42.4	09 13 43.04					1.23	0.16
125         SX2017xx <sup>2</sup> 0747 03.03         +26 46 25.8         0747 02.32         +26 46 34.7         0.0240         27.34         13.02         6.30         0.59           126         SX2017ph <sup>4</sup> 10 33 12.73         +36 11 24.6         03 33 13.19         +36 11 03.8         0.0151         49.91         21.53         6.63         0.83           128         SX2017ph <sup>4</sup> 10 03 33 12.73         +36 11 24.6         0.033         18.42         -22 10 30.7         -         44.52         0.0017         57.30         7.04         1.60         0.22           130         SX2018xr <sup>6</sup> 14 06 34.81         -32 34.44.1         14 06 35.05         -32 34 37.6         0.0339         58.63         7.07         4.44         5.0         0.014         8.22         2.40         0.67         0.025           133         SX2018dr4 <sup>6</sup> 13 38 38.47         +071 31.2         13 38 38.56         +071 25.94         0.0146         8.22         2.40         0.67         0.05           135         SX2018fcs <sup>6</sup> 0.04 05 5.77         -56 48.3         0.0250         1.87.4         8.30         1.62         0.21         1.83.8         1.81.2         1.83.8         1.83.8         1.81.3         5.00.16         <			01 12 38.19	$+05\ 45\ 58.4$	01 12 38.20	$+05\ 45\ 56.0$	0.0380			1.81	
126       SN2017yd <sup>b</sup> 11 46 25.00       +01 59 33.1       11 46 24.70       +01 59 39.6       00285       19.42       7.90       4.52       0.81         128       SN2017jdr <sup>b</sup> 10 23 45.51       +53 16 62.05       10 23 46.90       +53 16 62.80       00.317       45.51       14.59       9.2.4       0.64         120       SN2017mv <sup>b</sup> 09 57 20.97       -41 35 21.0       09 57 20.90       -41 35 28.0       00.117       77.30       7.04       1.69       0.23         131       SN2017mv <sup>b</sup> 09 57 20.97       -41 35 21.0       09 57 35.6       -721 24 37.6       0.0317       7.50       7.44       1.69       0.23         132       SN2018mv <sup>b</sup> 10 10 28.16       +021 34.88       10 10 27.86       +021 34.16       6.0217       58.49       6.70       0.05         134       SN2018mv <sup>b</sup> 03 52 0.77       -56.45 14.6       0.355 21.66       -56.44 46.6       0.0243       7.86       2.89       1.10       0.21         135       SN2018mv <sup>b</sup> 0.23 0.51       5.43       0.40       57.20       4.34       0.46       1.32       2.22       3.50       1.01       1.02       1.02       1.02       1.02       1.02       1.02       1.02 <td>124</td> <td></td> <td>07 10 41.07</td> <td><math>+06\ 27\ 41.4</math></td> <td>07 10 40.48</td> <td>+06 27 13.0</td> <td>0.0120</td> <td>39.64</td> <td>29.73</td> <td>7.30</td> <td>1.50</td>	124		07 10 41.07	$+06\ 27\ 41.4$	07 10 40.48	+06 27 13.0	0.0120	39.64	29.73	7.30	1.50
127         SN2017jμ <sup>b</sup> 0.0.31 2.73         +36 11 24.6         0.33 13.19         +36 11 03.8         0.0151         49.91         14.59         9.24         0.64           128         SN2017ju <sup>b</sup> 0.97 36.150         -22 10 23.91         0.97 36.41         -22 10 30.7         7.53         7.04         1.69         0.22           108         SN2017m <sup>b</sup> 1.06 35.10         -97 27.00         -41 35 28.0         0.0117         7.30         7.04         1.69         0.22           128         SN2018m <sup>b</sup> 1.06 34.81         -32 34.44.1         1.40 63.508         -32 34 37.6         0.0339         38.63         7.17         4.85         0.40           128         SN2018k <sup>b</sup> 1.01 2.81         8.80         0.62 7.10.7         0.060 4.84         -0.52 7.10.7         0.060 4.37.86         0.33 1.87         4.81         1.61         1.53           128         SN2018k <sup>b</sup> 1.05 5.70         -1.51 68.89         0.0250         4.63 1.83         1.62         1.10 8.13         1.83         1.82         1.10 8.22         1.83         1.61         1.23         1.83         1.83         1.83         1.83         1.83         1.83         1.83         1.83         1.83         1.83         1	125		07 47 03.03	$+26\ 46\ 25.8$	07 47 02.32	+26 46 34.7	0.0240	27.43	13.02	6.30	0.95
128         SN2017jark         10 23 45.1         +33 06 20.5         10 23 46.90         +53 06 28.0         0.0317         45.1         14.59         9.2.4         0.64           130         SN2017ms <sup>k</sup> 0.9 57 20.97         -41 35 21.0         0.9 57 20.90         -41 35 28.0         0.0117         57.30         7.04         1.69         0.23           131         SN2018ms <sup>k</sup> 1.01 02 16         +421 34.84         1.01 02.786         +421 34.16         0.0217         58.63         7.47         4.85         0.23           132         SN2018ms <sup>k</sup> 1.03 03.70         -0.527 10.29         1.40 63.489         -0.527 10.7         0.0095         137.4         8.30         1.62         0.12         1.53 88.46         +011 25.94         0.146         8.23         2.24         0.67         1.97         9.75         0.83           134         SN2018ms <sup>k</sup> 0.05 52.0         -15.05 8.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250         4.53 85.90         0.250<						+01 59 39.6					
129       SN2017 μ <sup>b</sup> 09 57 36.150       -22 10 23.01       09 57 36.41       -22 10 30.7         131       SN2018ark <sup>a</sup> 14 06 34.81       -32 34 44.1       14 06 35.05       -32 34 37.6       0.0339       55.63       7.17       4.85       0.02         131       SN2018ark <sup>b</sup> 14 06 34.84       10 10 27.86       +00 13 41.6       0.0217       55.63       8.49       3.73       0.22         133       SN2018ark <sup>b</sup> 14 05 34.6       -00 13 41.6       0.0217       55.63       8.49       3.73       0.22         134       SN2018ark <sup>b</sup> 14 05 56.72       -15 08 43.6       04 05 55.00       -15 08 55.9       0.025       4.67       19.37       0.75       0.83         135       SN2018irk <sup>b</sup> 13 50 42.50       -15 08 55.9       0.025       4.67       19.37       1.63       1.63       1.63       1.22       3.35       1.10       0.22       3.33       1.61       0.22       3.35       1.61       0.23       3.33       1.63       1.22       3.43       1.63       1.22       3.45       1.63       1.22       3.64       1.63       1.22       3.64       1.63       1.22       3.64       1.41       1.55       0.0046       1.42 <td></td> <td>5</td> <td></td> <td></td> <td></td> <td>+36 11 03.8</td> <td></td> <td></td> <td></td> <td></td> <td></td>		5				+36 11 03.8					
130       SN2017mw <sup>1</sup> 09 57 20.97       -41 35 21.0       09 57 20.90       -41 35 28.0       0.0117       57.30       7.04       1.69       0.25         131       SN2018me <sup>1</sup> 10 10 28.16       +02 13 48.8       10 10 27.86       +02 13 41.6       0.0217       58.63       8.49       3.73       0.29         131       SN2018me <sup>1</sup> 13 88 3847       +07 13 10.12       13 58 38.56       +01 12 59.4       0.0146       82.82       2.24       0.67       0.05         134       SN2018me <sup>1</sup> 14 06 54.70       -05 27 10.57       14 06 54.59       -15 08 58.90       0.0250       46.57       19.37       9.75       0.83         135       SN2018me <sup>1</sup> 14 05 31.77       -56 45 14.6       03 55 2071       -56 44 46.6       0.0243       37.86       2.8.94       14.18       1.53         138       SN2018me <sup>1</sup> 12 0.37.8       +41 15 56.5       12 10.53.7       +41 13 15.5.0       0.0168       42.48       11.51       3.93       0.54       0.44         140       SN2018me <sup>1</sup> 08 20 17.38       +41 35.54.7       0.055.90       +25 3 3.6.8       -22       2.55       0.54       0.44         141       SN2018me <sup>1</sup> 08 20 17.38       +42 13 54.							0.0317	45.51	14.59	9.24	0.64
131       SN2018ar <sup>4</sup> 14 06 34.81       -32 34 44.1       14 06 330.5       -32 34 37.6       0.0339       58.63       7.17       4.85       0.02         133       SN2018kdt <sup>2</sup> 10 58.16       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 58 38.67       +07 13 01.2       13 68 38.00       16.6 20.12       2.04       0.014       33 74.5       2.244       0.67       0.03       0.014       33 78.6       2.244       1.18       15.3       33 78.6       2.244       1.18						$-22\ 10\ 30.7$					
122       SN2018.bsg <sup>h</sup> 10       10       12       44       0.0217       58.63       8.49       3.73       0.29         134       SN2018.dtg <sup>h</sup> 14       65.43       -0.5       712.59.4       0.0146       82.82       2.24       0.67       0.05         134       SN2018.ts <sup>2+</sup> 14.05       65.72       -15.08       45.80       0.0250       46.57       19.37       97.5       0.83         135       SN2018.ts <sup>2+</sup> 0.05       23.59       42.90       +34.20       23.99       23.59       42.90       +34.20       2.22       3.35       1.01       0.21         138       SN2018.ts <sup>2+</sup> 0.0231       17.81       15.55       0.044       134.32       122.46       1.41.8       1.55       1.21       4.33       1.22       3.35       1.01       0.21       1.42.8       1.41.8       1.35       1.22.46       0.045       1.44.14       1.41.8       1.55       1.21.65       1.33       1.22.46       1.43.15.60       0.0500       2.8.72       0.55       0.54       0.04         141       SN2018.ts <sup>2+</sup> 0.83.14       1.43.53       1.34.54       5.53.12       0.01       1.55       0.55       0.55       0											
133       SN20184dr <sup>2</sup> 13 58 38.47       +07 13 01.2       13 58 38.56       +07 12 59.4       0.0146       S2.82       2.24       0.67       0.05         134       SN201816x <sup>4</sup> 04 05 56.72       -15 08 43.6       04 06 55.90       -15 08 58.9       0.0250       46.57       19.37       9.75       0.83         136       SN201816x <sup>4</sup> 03 55 20.77       -56 45 14.6       03 55 21.66       -56 44 46.6       0.0233       37.66       28.94       14.18       15.3         137       SN20181x <sup>4</sup> 16 32 02.31       +78 12 40.9       16 32 39.20       +78 11 55.5       0.0044       3.222       3.55       0.54       0.0145         138       SN20181x <sup>4</sup> 12 16 33.78       +41 31 56.5       12 16 33.76       +41 41 35 6.0       0.0050       28.72       0.55       0.54       0.044         140       SN20181x <sup>4</sup> 12 16 33.78       +12 35 34.7       07 05 53.41       +12 53 34.6       0.0250       42.44       1.151       3.39       0.54         142       SN20181x <sup>4</sup> 07 05 33.44       +12 53 34.7       07 02 51 44.60       22.20       8.0       0.0376											
134       SN2018dfg <sup>2</sup> 140634.70       -05270.29       140634.89       -05271.07       0.0095       137.45       8.30       1.62       0.12         135       SN2018fax <sup>4</sup> 03552.0.77       -564514.6       035521.66       -564446.6       0.0250       46.57       19.37       9.75       0.83         136       SN2018fax <sup>4</sup> 03552.0.77       -564514.6       035521.66       -564446.6       0.0243       37.86       28.94       14.18       1.53         137       SN2018fax <sup>4</sup> 23.92.01       +73.155.5       0.0446       134.32       122.64       11.65       1.83         138       SN2018fax <sup>4</sup> 03.573.44       +12.533.6.       0.0500       28.72       0.55       0.54       0.044         143       SN2018fax <sup>6</sup> 09.53.44       +12.533.6.       0.0376       54.44       11.51       3.93       0.54         143       SN2018fax <sup>6</sup> 09.51.81.9       +34353.53.3       0.0385       38.74       9.53       7.27       0.49         144       SN2018fax <sup>6</sup> 0.95.14       +12.23.04.6       0.0376       54.54       22.29       1.16       14.22.29       0.0376       55.56       14.22.29       0.0376       55.56       14											
135       SN2018(ac <sup>1</sup> /c)       04 05 55.07.7       -5.08 41.66       04 05 55.90       -15 08 58.9       0.0250       46.57       19.37       9.75       0.033         136       SN20186µb <sup>2</sup> 23 59 42.80       +34 20 39.9       23 59 42.90       +34 20 42.6       0.0143       37.86       28.94       11.85       .021         138       SN2018µb <sup>2</sup> 16 32 02.31       +78 12 40.9       16 32 39.20       +78 11 53.5       0.0046       13.42       12.64       11.65       1.83         140       SN2018µb <sup>2</sup> 12 16 33.78       +41 31 56.5       12 16 33.76       +41 31 56.0       0.0500       28.72       0.55       0.54       0.044         141       SN2018µb <sup>2</sup> 07 05 53.44       +12 53 34.7       07 05 53.41       +12 53 36.8       -       -       -       -       -       -       -       -       -       -       0.0500       28.72       0.55       0.54       0.044         143       SN2018µb <sup>2</sup> 07 23 14.452       25 10.410       +40 90 664.3       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -											
136       SN20188c <sup>2</sup> 03 55 20.77       -56 45 14.6       03 55 21.66       -564 44.6.6       0.0148       37.86       2.8.94       14.18       1.53         137       SN20181b <sup>4</sup> 15 20 2.31       +78 12 40.9       16 32 39.20       +78 11 53.5       0.0046       134.32       12.64       11.65       1.8.3         139       SN20181b <sup>4</sup> 23 49 58.18       +07 04 23.7       23 49 58.17       +07 04 19.7											
137       SN2018pb <sup>4</sup> 23 59 42.00       +34 20 39       23 59 42.90       +34 20 42.6       0.0146       312.22       3.35       1.01       0.21         138       SN2018hhs <sup>3</sup> 23 49 58.18       +470 42 3.7       23 49 58.17       +070 41 9.7       1.153       0.0046       134 32       12.264       11.65       1.83         140       SN2018hhs <sup>3</sup> 12 16 33.78       +41 31 56.5       12 16 33.76       +41 31 56.0       0.050       28.72       0.55       0.54       0.044         141       SN2018hk <sup>30</sup> 07 05 53.44       +12 53 34.7       07 05 53.41       +12 53 36.8       0.0385       38.74       9.53       7.27       0.49         143       SN2018hc <sup>41</sup> 00 0832       +66 11 46.02       -       +22 29 10.11       16 23 26.24       +22 29 0.86       0.0376       -       -       -       -       -       148       SN2018hu <sup>41</sup> 10 0.0832       +22 29 10.11       16 23 26.21       +22 29 0.86       0.0376       -       -       -       -       -       0.0376       -       -       -       0.019       10 43.47       3.17       0.80       0.15       SN2019hu <sup>41</sup> 0.32 87.24       +46 60 72.18       0.0219 155       -       - <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
138       SN2018hg <sup>10</sup> 16 32 02.1       +78 12 40.9       16 32 39.0       +78 11 33.5       0.006       134.32       12.64       11.65       1.83         139       SN2018hg <sup>10</sup> 12 16 33.78       +41 31 56.5       12 16 33.76       +41 31 56.0       0.0500       28.72       0.55       0.54       0.044         141       SN2018hg <sup>10</sup> 00 55 3.44       +12 53 34.7       0.70 55 3.41       +12 53 34.8       0.95 18.13       +34 53 53.3       0.0385       38.74       9.53       7.27       0.49         143       SN2018hg <sup>10</sup> 00 55 14.44       +42 53 43.8       0.95 91 8.13       +34 53 53.3       0.0385       38.74       9.53       7.27       0.49         145       SN2018mg <sup>10</sup> 10 23 26.53       +22 29 10.1       16 23 26.24       +22 29 0.86       0.0376       -											
139       SN2018hpd*       23 49 Sk18       +07 (4 32,7)       23 49 Sk17       +07 (04 19,7)         140       SN2018hpd*       12 16 33,78       +41 31 56.5       12 16 33,76       +41 31 56.0       0.0500       28.72       0.55       0.54       0.04         141       SN2018hpd*       07 05 53,44       +12 53 34.7       07 05 53,41       +12 53 35.8       -       -       -       -       -       -       0.44         SN2018hpd*       07 05 13,44       +12 53 34.7       07 05 53,41       +12 53 35.8       -       -       -       -       -       0.44         SN2018hpd*       07 23 14.632       +56 31 30.45       07 23 14.63       +56 31 29.6       -		*									
140       SN2018hug <sup>b</sup> 12 16 33.78       +41 31 56.5       12 16 33.76       +41 31 56.0       0.0500       28.72       0.55       0.54       0.04         141       SN2018hug <sup>b</sup> 07 10 5 53.44       +12 53 34.7       07 10 5 53.44       +12 53 36.8       11.51       3.93       0.054         143       SN2018hug <sup>b</sup> 07 10 5 31.44.52       +56 31 30.45       +56 31 29.6       144       SN2018hug <sup>b</sup> 95 18 1.9       +34 53 33.3       0.0385       38.74       9.53       7.27       0.49         144       SN2018hug <sup>b</sup> 16 23 26.53       +22 29 10.1       16 23 26.24       +22 29 08.6       0.0376       -							0.0046	134.32	122.64	11.65	1.83
141       SN2018hyw <sup>h</sup> 08 20 17.38       +20 52 32.2       08 20 16.57       +20 52 30.3       0.0168       42.48       11.51       3.93       0.54         142       SN2018juk <sup>h</sup> 09 59 18.19       +34 53 33.3       0.0385       38.74       9.53       7.27       0.49         143       SN2018juk <sup>h</sup> 09 59 18.19       +34 53 35.3       0.0385       38.74       9.53       7.27       0.49         144       SN2018wc <sup>h</sup> 18 10 0.832       -65 13 0.45       07 23 14.45       +56 31 29.6       - <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
143       SN2018jak <sup>b</sup> 09 59 18.19       +34 53 43.8.       09 59 18.13       +34 53 53.3       0.0385       38.74       9.53       7.27       0.49         144       SN2018jac <sup>b</sup> 10 10 0.832       +56 31 30.45       07 23 14.45       +56 31 29.6       -		2					0.0168	42.48	11.51	3.93	0.54
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							0.0350	33.74	2.12	1.48	0.13
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175         PS1-14od <sup>b</sup> 03 21 06.23         -07 16 57.4         03 21 06.08         -07 16 56.8         0.0200         19.87         2.31         0.94         0.23           176         PS15apj <sup>b</sup> 18 28 58.24         +22 54 10.6         18 28 57.36         +22 54 11.0         0.0140         56.00         12.17         3.48         0.43           177         PS15bgt <sup>b</sup> 22 46 05.04         -10 59 48.4         22 46 03.70         -11 00 04.3         0.0089         125.36         25.34         4.63         0.40           178         PS15bgt <sup>b</sup> 17 04 32.29         +01 20 58.5         17 04 32.26         +01 20 47.7         0.0230         37.00         10.81         5.02         0.58					14 32 31.19	-13 39 26.0	0.0210	43.47	2.47	1.05	0.11
176         PS15apj <sup>b</sup> 18 28 58.24         +22 54 10.6         18 28 57.36         +22 54 11.0         0.0140         56.00         12.17         3.48         0.43           177         PS15bgt <sup>b</sup> 22 46 05.04         -10 59 48.4         22 46 03.70         -11 00 04.3         0.0089         125.36         25.34         4.63         0.40           178         PS15bgt <sup>b</sup> 17 04 32.29         +01 20 58.5         17 04 32.26         +01 20 47.7         0.0230         37.00         10.81         5.02         0.58						0		40.0-		0.0.1	0.55
177         PS15bgt <sup>b</sup> 22 46 05.04         -10 59 48.4         22 46 03.70         -11 00 04.3         0.0089         125.36         25.34         4.63         0.40           178         PS15bgt <sup>b</sup> 17 04 32.29         +01 20 58.5         17 04 32.26         +01 20 47.7         0.0230         37.00         10.81         5.02         0.58											
178 PS15bqc <sup>b</sup> 17 04 32.29 +01 20 58.5 17 04 32.26 +01 20 47.7 0.0230 37.00 10.81 5.02 0.58											
		U									
$1/9 \qquad P1F10ntz' \qquad 15\ 08\ 37.52 \qquad +79\ 47\ 13.2 \qquad 15\ 08\ 37.55 \qquad +79\ 47\ 13.3 \qquad 0.0352 \qquad 28.06 \qquad 0.13 \qquad 0.09 \qquad 0.01$											
	179	PTF10htz <sup>b</sup>	13 08 37.52	+79 47 13.2	13 08 37.55	+79 47 13.3	0.0352	28.06	0.13	0.09	0.01

*Notes.* <sup>*a*</sup> The value of  $D_{25}$  is measured as an isophotal level of 25 mag arcsec<sup>-2</sup> in the SDSS *g* band (Hakobyan et al. 2012, 2016).

<sup>b</sup>Candidates for type IIb supernovae.

<sup>c</sup>CSS151130:014258+273410.

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